In Lieu of
Form 3160
(June 1990)

## UNITED STATES DEPARTMENT OF INTERIOR **BUREAU OF LAND MANAGEMENT**

FORM APPROVED
Budget Bureau No. 1004-013:
Expires: March 31, 1993

If Unit or CA, Agreement Designation

SUNDRY NOTICE	AND	PEDUDIC	ONWELLS
SUMBET NUTLES	AINI	KEPUKIS	ON WELLS

Do not use this form for proposals to drill or to deepen or reentry to a different reservoir. Use "APPLICATION TO DRILL" for permit for such proposals

Lease Designation and Serial No. SF-078769

6. If Indian, Allottee or Tribe Name

		JCATE.

8. Type of Well Oil Well X Gas Well

Well Name and No. **ROSA UNIT #267A** 

Name of Operator

3.

4.

WILLIAMS PRODUCTION COMPANY

9. API Well No. 30-039-29519

5.

7.

Address and Telephone No.

PO BOX 3102 MS 25-2, TULSA, OK 74101 (918) 573-6254

Field and Pool, or Exploratory Area BASIN FRUITLAND COAL

Location of Well (Footage, Sec., T., R., M., or Survey Description) 1150' FNL & 30' FWL, NW/4 NW/4 SEC 28-T31N-R05W

County or Parish, State

11. RIO ARRIBA, NM

## CHECK APPROPRIATE BOX(s) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION				
Notice of Intent	Abandonment	Change of Plans			
	Recompletion	New Construction			
X Subsequent Report	Plugging Back	Non-Routine Fracturing			
	Casing Repair	Water Shut-Off			
Final Abandonment	Altering Casing	Conversion to Injection			
	Other Production Test	Dispose Water			
		(Note: Report results of multiple completion			
		on Well Completion or Recompletion Report			
		and Log form.)			

13. Describe Proposed or Completed Operations (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work. If well is directionally drilled, give subsurface locations and measured and true vertical depths for all markers and zones pertinent to this work.)\*

Attached is the IP test that was conducted on the above well on July 18, 2005.



			41.50	LAUGUE	
14.	I hereby certify that the foregoing is true and correct				
	Signed Tracy Ross Tracy Ross	Title Sr. Production Analyst	Date	January 5,	2006 PACCEPTED FOR RECORD
	(This space for Federal or State office use)				
	Approved by	Title		Date	JAN 1 1 2006
	Conditions of approval, if any:				FARMINGTON FIELD OFFICE BY

Title 18 U.S.C. Section 1001, makes it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

## NEW MEXICO OIL CONSERVATION COMMISSION MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Tubing Size	Operator						Lease or Unit	Name			
A initial   Annual   Special   7/18/2005   Blevation   G414*   Unit   Sec   Typ   Reg						ROSA UNIT					
Completion Date		Test Type Test Date									
Title   Titl	X In	itial A	nnual	Special		7/18/2005		#2	267A (API	# 30-039-2951	l <b>9</b> )
Casing Size	Completion	Date	Total Depth		Plug Back T	D	1		l .		Rng
S-1/2"   17#   3610'   3390' - 3512'   Pool	7/14	/2005	36	10'			64	14'	D	28 31N	5W
Tubing   Size   2-78"   6.5#   d   3534'   Perforations:   3534'   Packer Set At   Formation   FT   Formation   FT   FT   FT   FT   FT   FT   FT   F	Casing Size		Weight	d	Set At	Perforations:			County		
Type Well - Single-Bradenhead-GG or GO Multiple   Packer Set At	5-:	1/2''	17#		3610'		3390' - 3512			RIO ARRIBA	4 .
Provide   Single-Bradenhead-GG or GO Multiple   Packer Set At   Formation   FT	Tubing Size		Weight	d	Set At	Perforations:			Pool		
Producing Thru   Tubing   Reservoir Temp. oF   Mean Annual Temp. oF   Barometer Pressure - Pa   Connection					3534'					BASIN	
Producing Thru Tubing	Type Well -	Single-Brader	head-GG or G	O Multiple		Packer Set At			Formation		
Tubing						<u></u>				FT	
H	Producing T	hru	Reservoir Te	mp. oF	Mean Annua	l Temp. oF		Barometer I	Pressure - Pa	Connection	
NO   Size	Tu	bing			<u>.l</u>			<u> </u>			
Prover	L	Н	Gq	%CO2		%N2	%H2S		1	Meter Run	Taps
Prover   X Orifice   Cline   Size   Pressure   OF   Duration of   Flow   OF   Pressure   OF   Pressure   OF   Pressure   OF   Duration of   Pressure   OF   Pressure   OF   Pressure   OF   Duration of   Pressure   OF   Pressure   OF   Pressure   OF   Duration of   Pressure   OF   OF   Pressure   OF   OF   Pressure   OF   OF   OF   OF   OF   OF   OF   O						<u>L.</u>	<u></u>				
Line   Size   Pressure   p.s.i.q   Pressure   Pressur			FLOW	/ DATA			TUBIN		CASIN		
NO   Size	]	Prover	X Orifice			_		1 -		-	
SI		Line	Size		Pressure	oF	Pressure	oF	Pressure	oF	Duration of
1   10   68   65   1.0 hr 2   10   68   65   1.0 hr 3   1.0 hr 3   5   68   50   1.5 hrs 4   5   68   50   2.0 hrs 5   72   45   3.0 hrs 7   2   45   3.0 hrs 7   45   45   3.0 hrs 7   45   45   45   45   45   45   45		Size			p.s.i.q						<del></del>
2   10   68   65   1.0 hr     3   5   68   50   1.5 hrs     4   5   68   50   2.0 hrs     5   72   45   3.0 hrs     5   72   45   3.0 hrs     5   72   45   3.0 hrs     6   72   72   72   73     7   7   7   7   7   7   7   7   7	SI		2" X 3/4"								
S	1								1		
S								<u> </u>			1
S	<b></b>				1						
RATE OF FLOW CALCULATION   Pressure   Factor   Flow   Q,Mcfd								1			<del>                                     </del>
NO	5	ļ				l	<u> </u>	72	45	<u></u>	3.0 hrs
NO         Coefficient (24 Hours)         hwPm         Pressure Flow Flow Flow Flow Flow Flow Flow Flow					RATEC	F FLOW CAL	CULATION		·	T	,
NO         (24 Hours)         hwPm         Pm         FI         Fq         Factor, Fpv         Q,Mcfd           1         9.604         17         0.9887         1.29         1.004         209           2         3						ļ		1 -	1	_	i e
1       9.604       17       0.9887       1.29       1.004       209         2       3       4       5       4       4       5       4       5       6       4       6       7       7       8       2       2       1 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>i</td> <td>1</td> <td></td> <td></td> <td></td>							i	1			
2       3       Cas Liquid Hydrocarbon Ration       Mcf/bbl.         4       AP.I Gravity of Liquid Hydrocarbons       Deq.         1       A.P.I Gravity of Liquid Hydrocarbons       Deq.         2       Specific Gravity Separator       Specific Gravity Flowing Fluid XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	<del>                                     </del>	ŀ	·			hwPm				<u> </u>	
NO			9.0	504		<u> </u>	17	0.9887	1.29	1.004	209
NO									ļ		<b>.</b>
NO         Pr         Temp. oR         Tr         Z         Gas Liquid Hydrocarbon Ration         Mcf/bbl.           1         A.P.I Gravity of Liquid Hydrocarbons         Deq.           2         Specific Gravity Separator         Specific Gravity Flowing Fluid xxxxxxxxxx         XXXXXXX           4         Specific Gravity Flowing Fluid xxxxxxxxxx         XXXXXXX           5         Critical Pressure         p.s.i.a.         p.s.i.a.           Critical Temperature         R         R           NO         Pt1         Pw         Pw²         Pc²-Pw²           1         57         3249         28080         Pc²-Pw²         (1) Pc² = 1.1157051 Pc²-Pw²         (2) Pc²-n = 1.0856           2         Absolute Open Flow         AOF = Q Pc²-n = Pc²-Pw²         AOF = Q Pc²-n = Slope, n         0.75           Remarks:         Approved By Commission:         Conducted By:         Calculated By:         Checked By:		_	<del> </del>								
1       A.P.I Gravity of Liquid Hydrocabrons       Deq.         2       Specific Gravity Separator       Specific Gravity Flowing Fluid XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX		<u> </u>	T = 5		т -	G 7: :177	<u> </u>	<u>.</u>			1
2       Specific Gravity Separator       XXXXXXX         3       Specific Gravity Flowing Fluid XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX		Pr	1emp. oR	l r	<u> </u>		·				
Specific Gravity Flowing Fluid xxxxxxxxxx		<u> </u>				-1	• •			<del></del>	Deq.
4         Critical Pressure         p.s.i.a.		<del> </del>	<del> </del>	<b>}</b>	<del> </del>		-				VXXXXXX
5         Critical Temperature         R        R           Pc         177         Pc²         31329         (1) Pc² = 1.1157051 (2) Pc²-n = 1.0856           NO         Pt1         Pw         Pw²         Pc²-Pw²         (1) Pc² = 1.1157051 (2) Pc²-n = 1.0856         1.0856           1         57         3249         28080         Pc²-Pw²         AOF = Q Pc²-n = 227         Pc²-Pw²         AOF = Q Pc²-n = Pc²-Pw²         227         Angle of Slope         Slope, n         0.75           Absolute Open Flow         227         Mcfd @ 15.025         Angle of Slope         Slope, n         0.75           Remarks:         Approved By Commission:         Conducted By:         Calculated By:         Checked By:		1	+		+	_					1
Pc         177         Pc²         31329         (1) Pc² = 1.1157051         (2) Pc²-n = 1.0856           NO         Pt1         Pw         Pw² Pc²-Pw²         (1) Pc² = 1.1157051         (2) Pc²-n = 1.0856           1         57         3249         28080         Pc²-Pw²         AOF = Q Pc²-n = Pc²-Pw²           3         AOF = Q Pc²-n = Pc²-Pw²         227         Angle of Slope = Slope = Slope = Slope = No.75           Absolute Open Flow         227         Mcfd @ 15.025         Angle of Slope = Slope = No.75         Slope, n No.75           Remarks:         Approved By Commission:         Conducted By:         Calculated By:         Checked By:				<del>                                     </del>	<del> </del>				<del></del>		1
NO         Pt1         Pw         Pw²         Pc²-Pw²         (1)         Pc² = 1.1157051         (2)         Pc²-n = Pc²-n = Pc²-Pw²         1.0856           1         57         3249         28080         Pc²-Pw²         AOF = Q         Pc²-Pw²         Pc²-Pw²         Pc²-Pw²         Pc²-Pw²         AOF = Q         Pc²-Pw²         Pc²-Pw²         Pc²-Pw²         Nogary         Pc²-Pw²         Pc²-Pw² <td< td=""><td></td><td>177</td><td>Do<sup>2</sup></td><td>21220</td><td>1</td><td>Citical Temp</td><td>ciature</td><td></td><td></td><td></td><td>1 K .</td></td<>		177	Do <sup>2</sup>	21220	1	Citical Temp	ciature				1 K .
1       57       3249       28080 $Pc^2-Pw^2$ $Pc^2-Pw^2$ 2       1       AOF = Q $Pc^2-Pw^2$ $Pc^2-Pw^2$ 3       AOF = Q $Pc^2-Pw^2$ $Pc^2-Pw^2$ Absolute Open Flow       227       Mcfd @ 15.025       Angle of Slope       Slope, n       0.75         Remarks:         Approved By Commission:       Conducted By:       Calculated By:       Checked By:			<del></del>		D-2 D-2	/41	n-2	1 1155051	(0)	D . 24	1.00=/
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	Pti		<del></del>		<sup>(۱)</sup>	$\frac{PC}{R^2 R^2} = \frac{2}{2}$	1.115/051	(2)	$\frac{Pc^{-1}n}{n} = \frac{1}{2}$	1.0856
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		<u> </u>	5/	3249	28080	-	Pc-Pw			Pc~-Pw	
Absolute Open Flow 227 Mcfd @ 15.025 Angle of Slope Slope, n 0.75  Remarks:  Approved By Commission: Conducted By: Calculated By: Checked By:		<del></del>			1	l	n 2.n	445			
Absolute Open Flow 227 Mcfd @ 15.025 Angle of Slope Slope, n 0.75  Remarks:  Approved By Commission: Conducted By: Calculated By: Checked By:		1		<b></b>		AOF = Q	<u>Pc^^" = </u>	<u>227</u>			
Remarks: Approved By Commission: Conducted By: Calculated By: Checked By:		<u></u>			1				1==-		
Approved By Commission: Conducted By: Calculated By: Checked By:		Open Flow	227	Mcfd @ 15.	025	Angle of Slop	е	<u>.</u>	Slope, n	0.75	
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Mark Lepich Tracy Ross	Approved B	y Commissior	<b>1</b> :	[Conducted ]	•			=	Checked By:		
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