# State of New Mexico Energy, Minerals and Natural Resources Department

Susana Martinez

Governor

Ken McQueen Cabinet Secretary David R. Catanach, Division Director
Oil Conservation Division



Matthias Sayer Deputy Cabinet Secretary

New Mexico Oil Conservation Division approval and conditions listed below are made in accordance with OCD Rule 19.15.7.11 and are in addition to the actions approved by BLM on the following 3160-3 APD form.

Operator Signature Date: _2/1/20/7
Well information;
Operator well Name and Number Kimbelo wish Und 1804
API#30-045-35830, Section 38, Township 25 NS, Range 9 E/W
Conditions of Approval: (See the below checked and handwritten conditions)  Notify Aztec OCD 24hrs prior to casing & cement.
Hold C-104 for directional survey & "As Drilled" Plat
Hold C-104 for NSL, NSP, DHC
<ul> <li>Spacing rule violation. Operator must follow up with change of status notification on other wel to be shut in or abandoned</li> </ul>
<ul> <li>Regarding the use of a pit, closed loop system or below grade tank, the operator must comply with the following as applicable:</li> </ul>
<ul> <li>A pit requires a complete C-144 be submitted and approved prior to the construction or use of the pit, pursuant to 19.15.17.8.A</li> </ul>
<ul> <li>A closed loop system requires notification prior to use, pursuant to 19.15.17.9.A</li> </ul>
<ul> <li>A below grade tank requires a registration be filed prior to the construction or use of the below grade tank, pursuant to 19.15.17.8.C</li> </ul>
<ul> <li>Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string</li> </ul>
O Submit Gas Capture Plan form prior to spudding or initiating recompletion operations
Regarding Hydraulic Fracturing, review EPA Underground Injection Control Guidance 84
Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system.
Well-bore communication is regulated under 19.15.29 NMAC. This requires well-bore Communication to be reported in accordance with 19.15.29.8.
Charles 6-9-2017
NMOCD Approved by Signature Date
1220 South St. Francis Drive • Santa Fe, New Mexico 87505

Phone (505) 476-3441 • Fax (505) 476-3462 • www.emnrd.state.nm.us/ocd

14

Form 3160 -3				FORM AP	PPROVED		
(March 2012)				OMB No. 1 Expires Octo	004-0137		
UNITED STATES DEPARTMENT OF THE I BUREAU OF LAND MAN				5. Lease Serial No. NMNM136267			
APPLICATION FOR PERMIT TO I				6. If Indian, Allotee or Tribe Name EASTERN NAVAJO			
la. Type of work:	R			7. If Unit or CA Agreement, Name and No. KIMBETO WASH UNIT / NMNM135255			
lb. Type of Well: Oil Well Gas Well Other	S	ingle Zone Multip	le Zone	8. Lease Name and Wel KWU 782H	I No.		
Name of Operator     WPX ENERGY LLC					35830		
720 S Main Aztec NM 87410	(505)333-	-		10. Field and Pool, or Exp	OS GAS POOL		
<ol> <li>Location of Well (Report location clearly and in accordance with any At surface SWSW / 407 FSL / 145 FWL / LAT 36.191801</li> <li>At proposed prod. zone SWSW / 746 FSL / 514 FWL / LAT</li> </ol>	/ LONG -1	107.802608	4	11. Sec., T. R. M. or Blk. a SEC 28 / T23N / R9W			
<ol> <li>Distance in miles and direction from nearest town or post office*</li> <li>37.8 miles</li> </ol>				12. County or Parish SAN JUAN	13. State NM		
15. Distance from proposed* location to nearest 20 feet property or lease line, ft. (Also to nearest drig. unit line, if any)	16. No. of 960	acres in lease	17. Spacin 960	g Unit dedicated to this well			
18. Distance from proposed location* to nearest well, drilling, completed, 145 feet applied for, on this lease, ft.	19. Propose 4387 feet	d Depth / 12702 feet		BIA Bond No. on file TB000178 / IND: B0015	576		
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 6540 feet	22. Approx 04/01/20 24. Atta	400	t*	23. Estimated duration 30 days	OIL CONS. DIV	DIST. 3	
The following, completed in accordance with the requirements of Onshore			tached to the		JIIN O 1 2	017	
<ol> <li>Well plat certified by a registered surveyor.</li> <li>A Drilling Plan.</li> <li>A Surface Use Plan (if the location is on National Forest System I SUPO must be filed with the appropriate Forest Service Office).</li> </ol>	•	Bond to cover the Item 20 above).     Operator certific	ne operation	ns unless covered by an exi		UIY	
25. Signature (Electronic Submission)		(Printed/Typed) by Granillo / Ph: (505	5)333-181	Da 0	te 2/01/2017		
Title Permitting Tech III							

KP

Approved by (Signature Title

Name (Printed/Typed)

**FARMINGTON** 

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Conditions of approval, if any, are attached.

Office

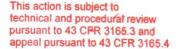
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

\*(Instructions on page 2)

DRILLING OPERATIONS AUTHORIZED ARE SUBJECT TO COMPLIANCE WITH ATTACHED "GENERAL REQUIREMENTS"

BLM'S APPROVAL OR ACCEPTANCE OF THIS ACTION DOES NOT RELIEVE THE LESSEE AND OPERATOR FROM OBTAINING ANY OTHER AUTHORIZATION REQUIRED FOR OPERATIONS ON FEDERAL AND INDIAN LANDS





District I 1625 N. French Drive, Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II B11 S. First Street, Artesia, NM BB210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Drive, Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department

Form C-102 Revised August 1, 2011

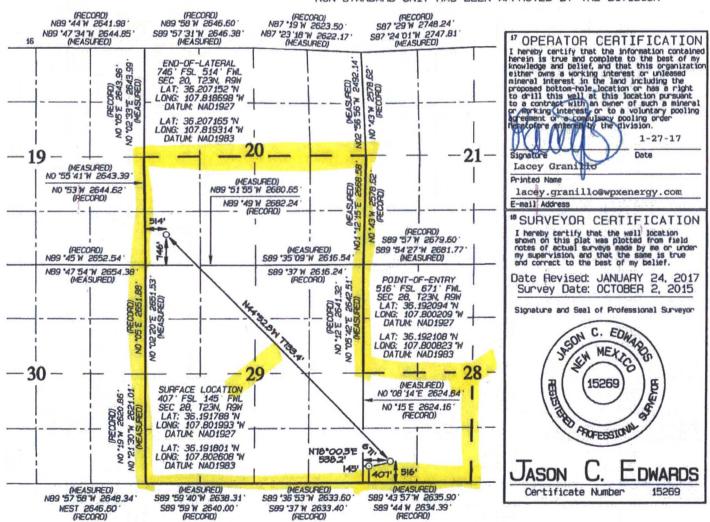
Submit one copy to Appropriate District Office

OTL CONSERVATION DIVISION AMENDED REPORT

# 1220 South St. Francis Drive Santa Fe. NM 87505

			WELL L	OCATIO	ON AND A	CREAGE D	EDIC	ATION PLA	T			
¹A	PI Numbe	Γ		Pool Coo	ie	11.0		Pool Nam	е			
20.04	5.3	583		97232	2		BASI	N MANCOS	GAS PO	DOL		
'Property 31614	Code		<u></u>			ty Name				· W	782H	er
'0GRID N 12078				WPX		tor Name PRODUCTION	N, LLC			•	Elevation 6540	
					10 Surface	e Location	1					
UL or lot no.	Section	Township	Range	Lot fan	Feet from the	North/South	h line	Feet from the	East/H	est line	Cr	ounty
М	28	23N	9₩		407	SOUT	H	145	WE	ST	SAN	JUAN
		1	1 Botto	m Hole	Location	If Differ	ent F	rom Surfac	е			
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South	h line	Feet from the	East/W	est line	Co	ounty
М	20	23N	9W		746	SOUT	H	514	WE	ST	SAN	JUAN
Dedicated Acres 1120.0	SW	/2 - Se /4 - Se	ection	28	<sup>13</sup> Joint or Infil	1 <sup>14</sup> Consolidation	Code	<sup>15</sup> Order No. R-1	4084			
	En	itire Se	ction a	29	110	ALL OWARLE	LITE	DE ACCIONE	TO TO	UTC CO	MOI ETT	IAON

NO ALLOWABLE WILL BE ASSIGNED TO THIS COMPLETION UNTIL ALL INTERESTS HAVE BEEN CONSOLIDATED OR A NON-STANDARD UNIT HAS BEEN APPROVED BY THE DIVISION





# **WPX Energy**

### **Operations Plan**

(Note: This procedure will be adjusted onsite based upon actual conditions)

Date:

January 26, 2017

Field:

**Basin Mancos** 

**Well Name:** 

KWU 782H

Surface:

SH Location:

SWSW Sec 28 23N-09W

Elevation: 6540' GR

**BH Location:** 

SWSW Sec 20 23N-09W

Minerals:

Measured Depth: 12,701.99'

# I. GEOLOGY

Surface formation - OJO ALAMO / KIRKLAND

#### A. FORMATION TOPS: (GR)

NAME	MD	TVD	NAME	MD	TVD
OJO ALAMO	22.00	22.00	POINT LOOKOUT	3,261.00	3,089.00
KIRTLAND	184.00	184.00	MANCOS	3,453.00	3,264.00
PICTURED CLIFFS	752.00	752.00	GALLUP	3,815.00	3,603.00
LEWIS	837.00	836.00	KICKOFF POINT	3,617.76	3,414.42
CHACRA	1,056.00	1,053.00	TOP TARGET	4,859.00	4,333.00
CLIFF HOUSE	2,242.00	2,160.00	LANDING POINT	4,968.52	4,342.94
MENEFEE	2,261.00	2,177.00	BASE TARGET	4,968.52	4,342.94
		8	TD	12,701.99	4,387.00

#### **B. MUD LOGGING PROGRAM:**

Mudlogger on location from surface csg to TD.

#### C. LOGGING PROGRAM:

LWD GR from surface casing to TD.

#### **D. NATURAL GAUGES:**

Gauge any noticeable increases in gas flow. Record all gauges in Tour book and on morning reports.

# II. DRILLING

# A. MUD PROGRAM:

LSND mud (WBM) will be used to drill the 12-1/4" Surface hole, the 8 3/4" Directional Vertical hole, and the curve portion of the wellbore. A LSND (WBM) or (OBM) will be used to drill the lateral portion of well. Treat for lost circulation as necessary. Obtain 100% returns prior to cementing. Notify Engineering of any mud losses.

# **B. BOP TESTING:**

While drill pipe is in use, the pipe rams and the blind rams will be function tested once each trip. The BOPE will be tested to 2,000 psi (High) for 10 minutes and the annular tested to 1,500 psi for 10 minutes. Pressure test surface casing to 1,500 psi for 30 minutes and intermediate casing to 1,500 psi for 30 minutes. Utilize a BOPE Testing Unit with a recording chart and appropriate test plug for testing. All tests and inspections will be recorded in the tour book as to time and results.

#### III. MATERIALS

# A. CASING PROGRAM:

CASING TYPE	OH SIZE (IN)	DEPTH (MD)	CSG SIZE	WEIGHT	GRADE	CONN
SURFACE	12.25"	320.00'	9.625"	36 LBS	J-55 or equiv	STC
INTERMEDIATE	8.75"	4,968.52'	7"	23 LBS	J-55 or equiv	LTC
PRODUCTION	6.125"	4818.52' - 12,701.99'	4.5"	11.6 LBS	P-110 or equiv	LTC
TIE BACK	6.125"	Surf 4818.52'	4.5"	11.6 LBS	P-110 or equiv	LTC

# **B. FLOAT EQUIPMENT:**

#### 1. SURFACE CASING:

9-5/8" notched regular pattern guide shoe. Run (1) standard centralizer on each of the bottom (4) joints of Surface Casing.

#### 2. INTERMEDIATE CASING:

7" cement nose guide shoe with a self-fill insert float. Place float collar one joint above the shoe. Install (1) centralizer on each of the bottom (3) joints and one standard centralizer every (3) joints to 2,500 ft. Run (1) centralizer at 2,500 ft., 2,300ft., 2,000ft., 1,500 ft., and 1,000 ft. If losses are encountered during the drilling of the intermediate section a DV tool will be utalized and a 2 stage cement job may be planned to ensure cement circ back to surface. The DV tool will be placed 100' above the top of the Chacra formation. If cement is circulated back to surface on the first stage, a cancelation device will be dropped to shift the dv tool closed and the 2nd stage cement job will be aborted at that time, if no cement is seen at surface on the 1st stage the stage tool will be opend and a 2nd stage cement job will be pumped.

#### 3. PRODUCTION LINER:

Run 4-1/2" Liner with cement nose guide Float Shoe + 2jts. of 4-1/2" casing + Landing Collar + 4-1/2" pup joint + 1 RSI (Sliding Sleeve) positioned inside the 330ft Hard line. Centralizer program will be determined by Wellbore condition and when Lateral is evaluated by Geoscientists and Reservoir Engineers. Set seals on Liner Hanger. Test TOL to 1500 psi for 15 minutes.

# C. CEMENT:

(Note: Volumes may be adjusted onsite due to actual conditions)

#### 1. Surface:

5 bbl Fresh Water Spacer, 100 sx (160 cu.ft.) of 14.5 ppg Type I-II (Neat G) + 20% Fly Ash cement w/ 7.41 gal/sack mix water ratio @ 1.61 cu ft/sx yield. Calculated @ volume + 50% excess. WOC 12 hours. Test csg to 600psi. Total Volume: (160 cu-ft/100 sx/ Bbls).TOC at Surface.

# 2. Intermediate:

Spacer #1: 20 bbl (112 cuft) Chemwash. Lead Cement: 87 bbls, 249 sks, (491 cuft), 12.3 ppg @ 1.97 cuft/sk yield. Tail Cement: 59 bbls, 254 sks, (331 cuft), 13.5 ppg @ 1.3 cuft/sk yield. Displacement: Displace w/ +/- 196 bbl Drilling mud or water. Total Cement: 146 bbls, 504 sks, (822 cuft)

#### 3. Prod Liner:

Spacer #1:10 bbl (56.cu-ft) Water Spacer. Spacer #2: 40 bbl 9.5 ppg (224.6 cu-ft) Tuned Spacer III. Spacer #3: 10 bbl Water Spacer. Lead Cement: Extencem ™ System. Yield 1.36 cuft/sk 13.3 ppg (772 sx /1050 cuft /187 bbls). Tail Spacer: 20 BBL of MMCR. Displacement: Displace w/ +/-172bbl Fr Water. Total Cement (772 sx /1050bbls).

#### D. COMPLETION:

Run CCL for perforating

#### A. PRESSURE TEST:

1. Pressure test 4-1/2" casing to 4500 psi max, hold at 1500 psi for 30 minutes. Increase pressure to Open RSI sleeves.

#### **B. STIMULATION:**

- 1. Stimulate with approximately 2,805,000# 20/40 mesh sand and 340,000# 16/30 mesh sand in 619,113 gallons water with 42,696 mscf N2 for 17 stages.
- 2. Isolate stages with flow through frac plug.
- 3. Drill out frac plugs and flowback lateral.

#### C. RUNNING TUBING:

1. <u>Production Tubing:</u> Run 2-7/8", 6.5#, J-55, EUE tubing with a SN on top of bottom joint. Land tubing near Top of Liner.

If this horizontal well is drilled past the applicable setbacks, an unorthodox location application is not required because the completed interval in this well, as defined by 19.15.16.7 B(1) NMAC, will be entirely within the applicable setbacks. This approach complies with all applicable rules, including 19.15.16.14 A(3) NMAC, 19.15.16.14 B(2) NMAC, 19.15.16.15 B(2) NMAC, and 19.15.16.15. B(4) NMAC.

#### **NOTES:**

A 4-1/2" 11.6# P-110 Liner will be run to TD and landed +/- 150 ft. into the 7" 23# J-55 Intermediate casing with a Liner Hanger and pack-off assembly then cemented to top of liner hanger.

After cementing and TOL clean up operations are complete, the TOL will be tested to 1500 psi (per BLM).

# **WPX Energy**

T23N R9W 2309-28M WLU-KWU Kimbeto Wash UT #782H - Slot A2

Wellbore #1

Plan: Design #2 27Sept16 sam

# **Standard Planning Report**

27 September, 2016

#### **WPX**

#### Planning Report

Database: COMPASS WPX Energy Company: Project: **T23N R9W** 2309-28M WLU-KWU Site:

Well: Kimbeto Wash UT #782H Wellbore #1

Wellbore: Design #2 27Sept16 sam Design:

Local Co-ordinate Reference: TVD Reference:

MD Reference: North Reference:

**Survey Calculation Method:** 

Well Kimbeto Wash UT #782H (A2) - Slot A2

GL @ 6540,00usft (Original Well Elev) GL @ 6540.00usft (Original Well Elev)

Minimum Curvature

**T23N R9W** Project

Map System:

Site Position:

Site

US State Plane 1927 (Exact solution)

NAD 1927 (NADCON CONUS)

System Datum:

Mean Sea Level

Geo Datum: Map Zone:

New Mexico West 3003

2309-28M WLU-KWU

Мар

Northing: Easting:

1,889,053.53 usft 509,247.80 usft

Latitude: Longitude:

36.191788

From: **Position Uncertainty:** 

0.00 usft

Slot Radius:

13.200 in

**Grid Convergence:** 

-107.801993

0.02°

Kimbeto Wash UT #782H - Slot A2 Well

**Well Position** 

+N/-S +E/-W 0.00 usft 0.00 usft Northing: Easting:

1,889,053.53 usft 509,247.80 usft Latitude: Longitude:

36.191788 -107.801993

**Position Uncertainty** 

0.00 usft

Wellhead Elevation:

0.00 usft

Ground Level:

6,540.00 usft

Wellbore #1 Wellbore Magnetics **Model Name** Sample Date Declination Dip Angle Field Strength (nT) **IGRF2015** 5/4/2016 9.33 62.88 49,837

Design #2 27Sept16 sam Design

**Audit Notes:** 

Version:

Phase:

PLAN

Tie On Depth:

0.00

**Vertical Section:** Depth From (TVD) +N/-S +E/-W (usft) 0.00

(usft) 0.00

(usft) 0.00

Direction (bearing) 318.62

Measured Depth (usft)	Inclination (°)	Azimuth (bearing)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°) Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
1,710.13	24.20	114.19	1,674.46	-103.20	229.69	2.00	2.00	0.00	114.19
3,617.76	24.20	114.19	3,414.42	-423.72	943.06	0.00	0.00	0.00	0.00
4,538.32	60.00	315.14	4,207.66	-173.26	809.97	9.00	3.89	-17.28	-161.82 Start 60 Tan #782
4,638.32	60.00	315.14	4,257.66	-111.87	748.88	0.00	0.00	0.00	0.00 End 60 Tan #782
4,803.55	74.87	315.14	4,320.89	-4.02	641.55	9.00	9.00	0.00	0.00
4,968.52	89.72	315.14	4,342.94	111.54	526.56	9.00	9.00	0.00	0.00 POE #782H
12,701.99	89.63	315.14	4,387.00	5,593.14	-4.928.41	0.00	0.00	0.00	-178.68 BHL #782H

# WPX

# Planning Report

Database: Company: Project: Site:

COMPASS WPX Energy T23N R9W 2309-28M WLU-KWU

Design #2 27Sept16 sam

Well: Kimbeto Wash UT #782H
Wellbore: Wellbore #1

Local Co-ordinate Reference:
TVD Reference:
MD Reference:
North Reference:
Survey Calculation Method:

Well Kimbeto Wash UT #782H (A2) - Slot A2 GL @ 6540.00usft (Original Well Elev) GL @ 6540.00usft (Original Well Elev)

True

Minimum Curvature

**Planned Survey** 

Design:

9 5/8"  500.00 0.00 0.00 500.00 0.00 0.00 0.00	Measured Depth (usft)	Inclination (°)	Azimuth (bearing)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9.58°   Start Build 2.00   0	0.00			0.00		0.00		0.00	0.00	0.0
Start Build 12.00	320.00	0.00	0.00	320.00	0.00	0.00	0.00	0.00	0.00	0.0
Start Build 2.00	9 5/8"									
1,000.00	500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.0
1,500.00	Start Build	2.00								
1,710.13	1,000.00	10.00	114.19	997.47	-17.84	39.70	-39.63	2.00	2.00	0.00
Hold 24.20 Inclination	1,500.00	20.00	114.19	1,479.82	-70.81	157.59	-157.31	2.00	2.00	0.00
Hold 24.20 Inclination	1 710 12	24 20	114 10	1 674 46	102 20	220.60	220.20	2.00	2.00	0.0
2,000.00			114.19	1,074.40	-103.20	229.09	-229.28	2.00	2.00	0.00
2,500.00		ing the section of th	444.40	4.000.05	454.00	200.00	227.42			
3,000.00			A.C. 0.0.00	C1 4 C1						0.0
3,500.00										0.0
3,617.76				1. 10 to 10						0.0
Start Build DLS 9,00 TFO -161.82	3,500.00	24.20	114.19	3,307.00	-403.93	899.02	-897.42	0.00	0.00	0.0
4,000.00 13.43 343.55 3,785.85 -412.91 1,003.79 -973.42 9.00 -2.82 -34 4,500.00 56.59 315.75 4,187.53 -196.48 832.84 -698.02 9.00 8.63 -4 4,538.32 60.00 315.14 4,207.66 -173.26 809.97 -665.48 9.00 8.90 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	3,617.76	24.20	114.19	3,414.42	-423.72	943.06	-941.38	0.00	0.00	0.0
4,500.00 56.59 315.75 4,187.53 -196.48 832.84 -698.02 9.00 8.63 4.538.32 60.00 315.14 4,207.66 -173.26 809.97 -665.48 9.00 8.90 -44.538.32 60.00 315.14 4,257.66 -111.87 748.88 -579.03 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Start Build I	DLS 9.00 TFO -10	61.82							
4,538.32         60.00         315.14         4,207.66         -173.26         809.97         -665.48         9.00         8.90         -Hold 60.00 Inclination           4,638.32         60.00         315.14         4,257.66         -111.87         748.88         -579.03         0.00	4,000.00	13.43	343.55	3,785.85	-412.91	1,003.79	-973.42	9.00	-2.82	-34.1
4,538.32         60.00         315.14         4,207.66         -173.26         809.97         -665.48         9.00         8.90         -Hold 60.00 Inclination           4,638.32         60.00         315.14         4,257.66         -111.87         748.88         -579.03         0.00         0.00         0.00           Start Bull DLS 9.00 TFO 0.00           4,803.55         74.87         315.14         4,320.89         -4.02         641.55         -427.15         9.00         9.00         0.00           Start DLS 9.00 TFO 0.00           4,968.52         89.72         315.14         4,342.94         111.54         526.56         -264.43         9.00         9.00         0.00	4,500.00	56.59	315.75	4,187.53	-196.48	832.84	-698.02			-5.50
4,638.32       60.00       315.14       4,257.66       -111.87       748.88       -579.03       0.00       0.00       0.00         Start Build DLS 9.00 TFO 0.00         4,803.55       74.87       315.14       4,342.94       111.54       526.56       -264.43       9.00       9.00       0         CSTAIL DLS 9.00 TFO 0.00         4,969.00       89.72       315.14       4,342.94       111.88       526.22       -263.95       0.00       0.00       0.00       0         7"         5,000.00       89.72       315.14       4,343.10       133.85       504.36       -233.01       0.00       0.00       0.00         5,500.00       89.71       315.14       4,3445.58       488.27       151.68       266.06       0.00       0.00       0.00         6,000.00       89.71       315.14       4,348.12       842.68       -201.01       765.14       0.00       0.00       0.00         6,500.00       89.70       315.14       4,350.71       1,97.09       -553.69       1,264.21       0.00       0.00       0.00         7,500.00       89.69       315.14       4,356.04       1,905.92       -1,259.06				10.000						-1.5
Start Build DLS 9.00 TFO 0.00           4,803.55         74.87         315.14         4,320.89         -4.02         641.55         -427.15         9.00         9.00         0           Start DLS 9.00 TFO 0.00           4,968.52         89.72         315.14         4,342.94         111.54         526.56         -264.43         9.00         9.00         0           POE at 89.72 Inc 315.14 Deg           4,969.00         89.72         315.14         4,342.94         111.88         526.22         -263.95         0.00         0.00         0	Hold 60.00 I	nclination								
4,803.55       74.87       315.14       4,320.89       -4.02       641.55       -427.15       9.00       9.00       0         Start DLS 9.00 TFO 0.00         4,968.52       89.72       315.14       4,342.94       111.54       526.56       -264.43       9.00       9.00       0         POE at 89.72 Inc 315.14 Deg         4,969.00       89.72       315.14       4,342.94       111.88       526.22       -263.95       0.00       0.00       0.00         5,000.00       89.72       315.14       4,343.10       133.85       504.36       -233.01       0.00       0.00       0.00       0         6,000.00       89.71       315.14       4,345.58       488.27       151.68       266.06       0.00       0.00       0<	4,638.32	60.00	315.14	4,257.66	-111.87	748.88	-579.03	0.00	0.00	0.0
Start DLS 9.00 TFO 0.00           4,968.52         89.72         315.14         4,342.94         111.54         526.56         -264.43         9.00         9.00         0           POE at 89.72 Inc 315.14 Deg           4,969.00         89.72         315.14         4,342.94         111.88         526.22         -263.95         0.00         0.00         0           7"           5,000.00         89.72         315.14         4,343.10         133.85         504.36         -233.01         0.00         0.00         0.00         0	Start Build I	OLS 9.00 TFO 0.0	0							
Start DLS 9.00 TFO 0.00           4,968.52         89.72         315.14         4,342.94         111.54         526.56         -264.43         9.00         9.00         0           POE at 89.72 Inc 315.14 Deg           4,969.00         89.72         315.14         4,342.94         111.88         526.22         -263.95         0.00         0.00         0.00           7"           5,000.00         89.71         315.14         4,343.10         133.85         504.36         -233.01         0.00         0.00         0.00         0.00         5,500.00         89.71         315.14         4,345.58         488.27         151.68         266.06         0.00         0.	4,803,55	74.87	315.14	4.320.89	-4.02	641.55	-427.15	9.00	9.00	0.0
4,968.52       89.72       315.14       4,342.94       111.54       526.56       -264.43       9.00       9.00       0         POE at 89.72 Inc 315.14 Deg         4,969.00       89.72       315.14       4,342.94       111.88       526.22       -263.95       0.00       0.00       0.00       0	Start DLS 9	00 TFO 0.00								
POE at 89.72 Inc 315.14 Deg         4,969.00         89.72         315.14         4,342.94         111.88         526.22         -263.95         0.00         0.00         0.00           7"           5,000.00         89.72         315.14         4,343.10         133.85         504.36         -233.01         0.00         0.00         0.00           5,500.00         89.71         315.14         4,345.58         488.27         151.68         266.06         0.00         0.00         0.00           6,000.00         89.71         315.14         4,348.12         842.68         -201.01         765.14         0.00         0.00         0.00           6,500.00         89.70         315.14         4,350.71         1,197.09         -553.69         1,264.21         0.00         0.00         0.00           7,500.00         89.69         315.14         4,356.04         1,905.92         -1,259.06         2,262.36         0.00         0.00         0.00           8,000.00         89.68         315.14         4,356.78         2,260.33         -1,611.74         2,761.43         0.00         0.00         0.00           9,000.00         89.67         315.14         4,364.31         2,969.14		the state of the s	315.14	4.342.94	111.54	526.56	-264.43	9.00	9.00	0.00
4,969.00       89.72       315.14       4,342.94       111.88       526.22       -263.95       0.00       0.00       0.00         7"         5,000.00       89.72       315.14       4,343.10       133.85       504.36       -233.01       0.00       0.00       0.00         5,500.00       89.71       315.14       4,345.58       488.27       151.68       266.06       0.00       0.00       0.00         6,000.00       89.71       315.14       4,348.12       842.68       -201.01       765.14       0.00       0.00       0.00         6,500.00       89.70       315.14       4,350.71       1,197.09       -553.69       1,264.21       0.00       0.00       0.00         7,000.00       89.70       315.14       4,356.04       1,905.92       -1,259.06       2,262.36       0.00       0.00       0.00         7,500.00       89.69       315.14       4,358.78       2,260.33       -1,611.74       2,761.43       0.00       0.00       0.00         8,500.00       89.68       315.14       4,364.57       2,614.73       -1,964.43       3,260.51       0.00       0.00       0.00         9,500.00       89.67       315.14	POF at 89.7									
5,000.00         89.72         315.14         4,343.10         133.85         504.36         -233.01         0.00         0.0		The second second second second second		4 342 94	111 88	526.22	-263 95	0.00	0.00	0.00
5,000.00         89.72         315.14         4,343.10         133.85         504.36         -233.01         0.00         0.00         0.00         5,500.00         6,000.00         0.00		00.72	010.14	4,042.04	111.00	320.22	-203.33	0.00	0.00	0,00
5,500.00         89.71         315.14         4,345.58         488.27         151.68         266.06         0.00         0.00         0.00           6,000.00         89.71         315.14         4,348.12         842.68         -201.01         765.14         0.00		89.72	315 14	4 343 10	133.85	504.36	-233.01	0.00	0.00	0.00
6,000.00 89.71 315.14 4,348.12 842.68 -201.01 765.14 0.00 0.00 0.00 (6,500.00 89.70 315.14 4,350.71 1,197.09 -553.69 1,264.21 0.00 0.00 0.00 (7,000.00 89.70 315.14 4,353.35 1,551.51 -906.37 1,763.29 0.00 0.00 0.00 (7,500.00 89.69 315.14 4,356.04 1,905.92 -1,259.06 2,262.36 0.00 0.00 0.00 (8,000.00 89.68 315.14 4,358.78 2,260.33 -1,611.74 2,761.43 0.00 0.00 0.00 (8,000.00 89.68 315.14 4,361.57 2,614.73 -1,964.43 3,260.51 0.00 0.00 0.00 (9,000.00 89.67 315.14 4,364.41 2,969.14 -2,317.11 3,759.58 0.00 0.00 0.00 (9,000.00 89.67 315.14 4,367.30 3,323.55 -2,669.80 4,258.65 0.00 0.00 0.00 (9,000.00 89.66 315.14 4,370.24 3,677.95 -3,022.48 4,757.72 0.00 0.00 0.00 (10,500.00 89.66 315.14 4,373.23 4,032.36 -3,375.17 5,256.79 0.00 0.00 0.00 (11,500.00 89.64 315.14 4,379.36 4,741.16 -4,080.55 6,254.93 0.00 0.00 0.00 (12,000.00 89.64 315.14 4,379.36 4,741.16 -4,080.55 6,254.93 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	,			N. Carlotte						0.00
6,500.00         89.70         315.14         4,350.71         1,197.09         -553.69         1,264.21         0.00 <td< td=""><td></td><td></td><td></td><td>10.000000000000000000000000000000000000</td><td></td><td></td><td></td><td></td><td></td><td></td></td<>				10.000000000000000000000000000000000000						
7,000.00         89.70         315.14         4,353.35         1,551.51         -906.37         1,763.29         0.00         0.00         0.00           7,500.00         89.69         315.14         4,356.04         1,905.92         -1,259.06         2,262.36         0.00         0.00         0.00           8,000.00         89.68         315.14         4,358.78         2,260.33         -1,611.74         2,761.43         0.00         0.00         0.00           8,500.00         89.68         315.14         4,361.57         2,614.73         -1,964.43         3,260.51         0.00         0.00         0.00           9,000.00         89.67         315.14         4,364.41         2,969.14         -2,317.11         3,759.58         0.00         0.00         0.00           9,500.00         89.67         315.14         4,367.30         3,323.55         -2,669.80         4,258.65         0.00         0.00         0.00           10,000.00         89.66         315.14         4,370.24         3,677.95         -3,022.48         4,757.72         0.00         0.00         0.00           11,000.00         89.65         315.14         4,376.27         4,386.76         -3,727.86         5,755.86         0.00										0.00
7,500.00         89.69         315.14         4,356.04         1,905.92         -1,259.06         2,262.36         0.00         0.00         0.00           8,000.00         89.68         315.14         4,358.78         2,260.33         -1,611.74         2,761.43         0.00         0.00         0.00           8,500.00         89.68         315.14         4,361.57         2,614.73         -1,964.43         3,260.51         0.00         0.00         0.00           9,000.00         89.67         315.14         4,364.41         2,969.14         -2,317.11         3,759.58         0.00         0.00         0.00           9,500.00         89.67         315.14         4,367.30         3,323.55         -2,669.80         4,258.65         0.00         0.00         0.00           10,000.00         89.66         315.14         4,370.24         3,677.95         -3,022.48         4,757.72         0.00         0.00         0.00           10,500.00         89.66         315.14         4,373.23         4,032.36         -3,375.17         5,256.79         0.00         0.00         0.00           11,000.00         89.65         315.14         4,376.27         4,386.76         -3,727.86         5,755.86         0										0.0
8,000.00       89.68       315.14       4,358.78       2,260.33       -1,611.74       2,761.43       0.00       0.00       0         8,500.00       89.68       315.14       4,361.57       2,614.73       -1,964.43       3,260.51       0.00       0.00       0         9,000.00       89.67       315.14       4,364.41       2,969.14       -2,317.11       3,759.58       0.00       0.00       0         9,500.00       89.67       315.14       4,367.30       3,323.55       -2,669.80       4,258.65       0.00       0.00       0         10,000.00       89.66       315.14       4,370.24       3,677.95       -3,022.48       4,757.72       0.00       0.00       0         10,500.00       89.66       315.14       4,373.23       4,032.36       -3,375.17       5,256.79       0.00       0.00       0         11,000.00       89.65       315.14       4,376.27       4,386.76       -3,727.86       5,755.86       0.00       0.00       0         11,500.00       89.64       315.14       4,379.36       4,741.16       -4,080.55       6,254.93       0.00       0.00       0         12,000.00       89.64       315.14       4,382.51 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.0</td></td<>										0.0
8,500.00       89.68       315.14       4,361.57       2,614.73       -1,964.43       3,260.51       0.00       0.00       0         9,000.00       89.67       315.14       4,364.41       2,969.14       -2,317.11       3,759.58       0.00       0.00       0         9,500.00       89.67       315.14       4,367.30       3,323.55       -2,669.80       4,258.65       0.00       0.00       0         10,000.00       89.66       315.14       4,370.24       3,677.95       -3,022.48       4,757.72       0.00       0.00       0         10,500.00       89.66       315.14       4,373.23       4,032.36       -3,375.17       5,256.79       0.00       0.00       0         11,000.00       89.65       315.14       4,376.27       4,386.76       -3,727.86       5,755.86       0.00       0.00       0         11,500.00       89.64       315.14       4,379.36       4,741.16       -4,080.55       6,254.93       0.00       0.00       0         12,000.00       89.64       315.14       4,382.51       5,095.57       -4,433.24       6,754.00       0.00       0.00       0	10.00									0.0
9,000.00       89.67       315.14       4,364.41       2,969.14       -2,317.11       3,759.58       0.00       0.00       0         9,500.00       89.67       315.14       4,367.30       3,323.55       -2,669.80       4,258.65       0.00       0.00       0         10,000.00       89.66       315.14       4,370.24       3,677.95       -3,022.48       4,757.72       0.00       0.00       0         10,500.00       89.66       315.14       4,373.23       4,032.36       -3,375.17       5,256.79       0.00       0.00       0         11,000.00       89.65       315.14       4,376.27       4,386.76       -3,727.86       5,755.86       0.00       0.00       0         11,500.00       89.64       315.14       4,379.36       4,741.16       -4,080.55       6,254.93       0.00       0.00       0         12,000.00       89.64       315.14       4,382.51       5,095.57       -4,433.24       6,754.00       0.00       0.00       0	8,000.00	89.68	315.14	4,358.78	2,260.33	-1,611.74	2,761.43	0.00	0.00	0.00
9,000.00       89.67       315.14       4,364.41       2,969.14       -2,317.11       3,759.58       0.00       0.00       0         9,500.00       89.67       315.14       4,367.30       3,323.55       -2,669.80       4,258.65       0.00       0.00       0         10,000.00       89.66       315.14       4,370.24       3,677.95       -3,022.48       4,757.72       0.00       0.00       0         10,500.00       89.66       315.14       4,373.23       4,032.36       -3,375.17       5,256.79       0.00       0.00       0         11,000.00       89.65       315.14       4,376.27       4,386.76       -3,727.86       5,755.86       0.00       0.00       0         11,500.00       89.64       315.14       4,379.36       4,741.16       -4,080.55       6,254.93       0.00       0.00       0         12,000.00       89.64       315.14       4,382.51       5,095.57       -4,433.24       6,754.00       0.00       0.00       0	8,500.00	89.68	315.14	4,361.57	2,614.73	-1,964,43	3,260,51	0.00	0.00	0.00
9,500.00       89.67       315.14       4,367.30       3,323.55       -2,669.80       4,258.65       0.00       0.00       0         10,000.00       89.66       315.14       4,370.24       3,677.95       -3,022.48       4,757.72       0.00       0.00       0         10,500.00       89.66       315.14       4,373.23       4,032.36       -3,375.17       5,256.79       0.00       0.00       0         11,000.00       89.65       315.14       4,376.27       4,386.76       -3,727.86       5,755.86       0.00       0.00       0         11,500.00       89.64       315.14       4,379.36       4,741.16       -4,080.55       6,254.93       0.00       0.00       0         12,000.00       89.64       315.14       4,382.51       5,095.57       -4,433.24       6,754.00       0.00       0.00       0	9,000.00	89.67	315.14	4.364.41	2.969.14	,				0.00
10,000.00     89.66     315.14     4,370.24     3,677.95     -3,022.48     4,757.72     0.00     0.00     0       10,500.00     89.66     315.14     4,373.23     4,032.36     -3,375.17     5,256.79     0.00     0.00     0       11,000.00     89.65     315.14     4,376.27     4,386.76     -3,727.86     5,755.86     0.00     0.00     0       11,500.00     89.64     315.14     4,379.36     4,741.16     -4,080.55     6,254.93     0.00     0.00     0       12,000.00     89.64     315.14     4,382.51     5,095.57     -4,433.24     6,754.00     0.00     0.00     0										0.00
10,500.00     89.66     315.14     4,373.23     4,032.36     -3,375.17     5,256.79     0.00     0.00     0       11,000.00     89.65     315.14     4,376.27     4,386.76     -3,727.86     5,755.86     0.00     0.00     0       11,500.00     89.64     315.14     4,379.36     4,741.16     -4,080.55     6,254.93     0.00     0.00     0       12,000.00     89.64     315.14     4,382.51     5,095.57     -4,433.24     6,754.00     0.00     0.00     0				The second second						0.00
11,000.00     89.65     315.14     4,376.27     4,386.76     -3,727.86     5,755.86     0.00     0.00     0.00       11,500.00     89.64     315.14     4,379.36     4,741.16     -4,080.55     6,254.93     0.00     0.00     0.00       12,000.00     89.64     315.14     4,382.51     5,095.57     -4,433.24     6,754.00     0.00     0.00     0.00	and the second second									0.00
11,500.00 89.64 315.14 4,379.36 4,741.16 -4,080.55 6,254.93 0.00 0.00 0.00 12,000.00 89.64 315.14 4,382.51 5,095.57 -4,433.24 6,754.00 0.00 0.00 0.00										
12,000.00 89.64 315.14 4,382.51 5,095.57 -4,433.24 6,754.00 0.00 0.00	the second secon									0.00
				***************************************						0.00
12.500.00 89.63 315.14 4.385.70 5.449.97 -4.785.93 7.253.07 0.00 0.00 0	The second secon						an earl account and the			0.00
										0.00

# **WPX**

# Planning Report

Database: Company: Project:

Site:

Well:

Wellbore:

Design:

COMPASS

WPX Energy

T23N R9W 2309-28M WLU-KWU

Kimbeto Wash UT #782H Wellbore #1

Design #2 27Sept16 sam

Local Co-ordinate Reference:

TVD Reference:
MD Reference:

North Reference: Survey Calculation Method: Well Kimbeto Wash UT #782H (A2) - Slot A2

GL @ 6540.00usft (Original Well Elev) GL @ 6540.00usft (Original Well Elev)

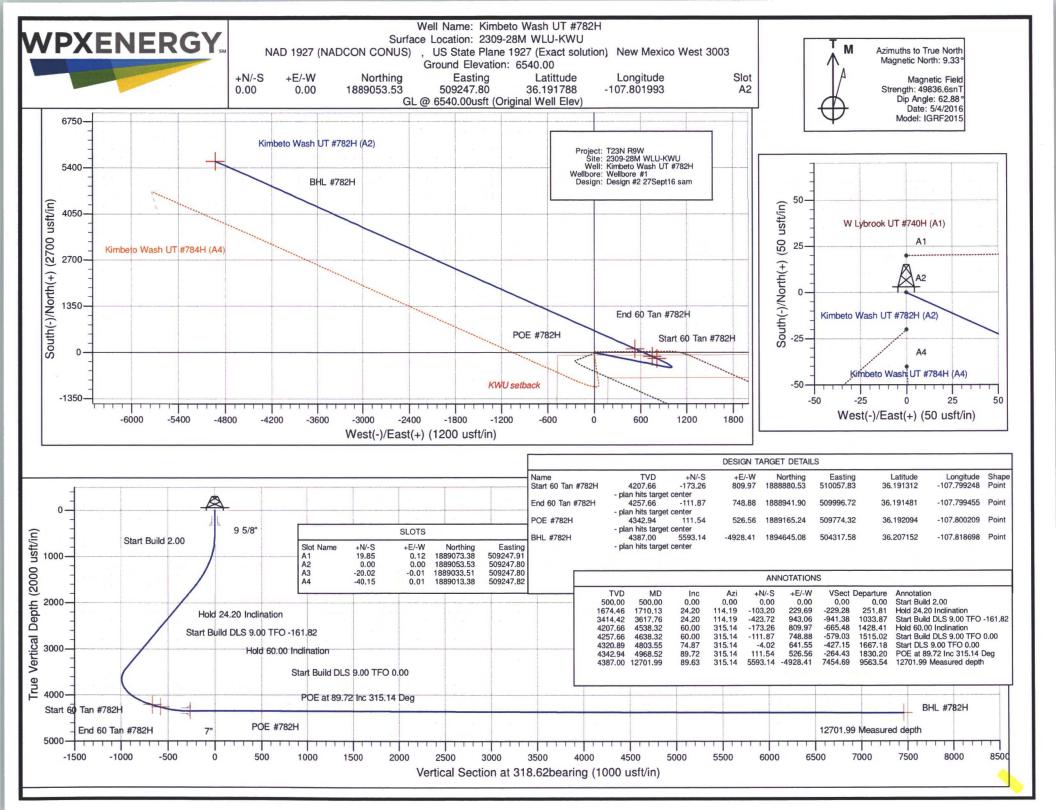
True

Minimum Curvature

Design Targets Target Name									
	ip Angle (°)	Dip Dir. (bearing	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
Start 60 Tan #782H - plan hits target center - Point	0.00	0.00	4,207.66	-173.26	809.97	1,888,880.53	510,057.83	36.191312	-107.799248
End 60 Tan #782H - plan hits target center - Point	0.00	0.00	4,257.66	-111.87	748.88	1,888,941.90	509,996.72	36.191481	-107.799455
POE #782H - plan hits target center - Point	0.00	0.00	4,342.94	111.54	526.56	1,889,165.24	509,774.33	36.192094	-107.800209
BHL #782H - plan hits target center - Point	0.00	0.00	4,387.00	5,593.14	-4,928.41	1,894,645.08	504,317.58	36.207152	-107.818699

Casing Points							
	Measured	Vertical Depth (usft)		Name	Casing Diameter (in)	Hole	
	320.00	320.00	9 5/8"		9.625	12.250	
	4,969.00	4,342.94	7"		7.000	8.750	

Measured	Vertical	Local Coor	dinates			
Depth	Depth	+N/-S	+E/-W			
(usft)	(usft)	(usft)	(usft)	Comment		
500.00	500.00	0.00	0.00	Start Build 2.00		
1,710.13	1,674.46	-103.20	229.69	Hold 24.20 Inclination		
3,617.76	3,414.42	-423.72	943.06	Start Build DLS 9.00 TFO -161.82		
4,538.32	4,207.66	-173.26	809.97	Hold 60.00 Inclination		
4,638.32	4,257.66	-111.87	748.88	Start Build DLS 9.00 TFO 0.00		
4,803.55	4,320.89	-4.02	641.55	Start DLS 9.00 TFO 0.00		
4,968.52	4,342.94	111.54	526,56	POE at 89.72 Inc 315.14 Deg		
12,701.99	4,387.00	5,593,14	-4,928.41	12701.99 Measured depth		



Road #7890, and follow along the W Lybrook UT 720H access for 3,123.1 feet to fork in the access. Trucks would take a left and continue westerly, which would be straight, following along WPX's W Lybrook UT 726H access for 3,937.3 feet to a fork in the access road. They would then take a left (westerly), which would be straight, following along the W Lybrook UT 730H planned access for 10,164.2 feet. They would take a left (south-westerly), which is straight, following along WPX's W Lybrook UT #738H planned access for 1,267.1 feet to the beginning of proposed Access Road #1. Trucks would proceed 2,491.4 feet along the newly constructed Access Road corridor #1 to WPX's KWU 782H/784H and W Lybrook Unit 740H/741H well pad.

# 6. CONSTRUCTION MATERIALS

The construction phase of the project would commence upon receipt of the approved APDs. The BLM-FFO would be notified (505-564-7600) at least 48 hours prior to the start of construction activities associated with the project. The construction phase of the project is anticipated to last approximately 3 to 4 weeks.

Construction and maintenance activities would cease if soil or road surfaces become saturated to the extent that construction equipment is unable to stay within the project area and/or when activities cause irreparable harm to roads, soils, or streams. Surfacing material, such as sandstone, would be used if economically viable and would be obtained from a permitted location.

The Natural Resources Conservation Service (NRCS) has mapped the soils in the proposed KWU 782H/784H and W Lybrook Unit 740H/741H Project area. Complete soil information is available in the NRCS's *Soil Survey of San Juan County, New Mexico, Eastern Part* (USDA/NRCS 2015). The soil map unit within the proposed project area footprint is described in the sections below.

# A. Fruitland-Persayo-Sheppard complex (hilly)

The entire project area encompasses this soil type. The project would include a moderate to large cut and fill within this soil type in order to construct the well pad. This would entail a maximum cut of 11 feet on the north end and a maximum fill of 9 feet on the northeast corner (corner 5) of the pad.

The Fruitland-Persayo-Sheppard complex (hilly) is composed of 40 percent Fruitland and similar soils, 30 percent Persayo and similar soils, and 25 percent Sheppard and similar soils. Fruitland-Persayo-Sheppard complex (hilly) soils are found on alluvial fans, stream terraces, hills, ridges, breaks, and dunes ranging from 4,000 feet to 6,400 feet in elevation. Fruitland soils occur on slopes of 5 to 30 percent, are well drained, and have a high water permeability. Persayo soils occur on slopes of 5 to 30 percent, are well drained, and have low to moderately high water permeability. Sheppard soils occur on slopes of 5 to 30 percent, are excessively drained, and have high to very high water permeability. This soil complex has a low to moderate potential for water erosion and moderate to high potential for wind erosion. The Fruitland-Persayo-Sheppard complex (hilly) is generally found within sandy, shale hills, and deep sand ecological sites (USDA/NRCS 2015).

# 7. METHODS FOR HANDLING WASTE

#### A. Cuttings

- Drilling operations would utilize a closed-loop system. Drilling of the horizontal laterals would be accomplished with water-based mud. All cuttings would be placed in roll-off bins and hauled to a commercial disposal facility or land farm. WPX would follow Onshore Oil and Gas Order No. 1 regarding the placement, operation, and removal of closed-loop systems. No blow pit would be used.
- Closed-loop tanks would be adequately sized for containment of all fluids.

# B. Drilling Fluids

Drilling fluids would be stored onsite in above-ground storage tanks. Upon termination of drilling operations, the drilling fluids would be recycled and transferred to other permitted closed-loop systems or returned to the vendor for reuse, as practical. All residual fluids would be hauled to a commercial disposal facility.

# C. Spills

