

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		1-17-78	
Company				Connection							
Great Lakes Chemical Corp.				C							
Pool				Formation				Unit			
Blanco				Mesa Verde							
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name			
1-8-78		4686		4629		6110' KB		Hammond			
Cog. Size	Wi.	d	Set At	Perforations:				Well No.			
				From 4460' KB To 4532' KB				5			
Thg. Size	Wi.	d	Set At	Perforations:				Unit Sec. Twp. Rge.			
1 1/2	2.9	1.61	4488' KB	From Open Ended To				F 35 27N 8W			
Type Well - Single - Bladenhead - G.G. or G.O. Multiple								Packer Set At		County	
Single										San Juan	
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Base Press. - P _g		State			
Tubing		114 # 4686		60		12.0		New Mexico			
L	H	G _g	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps			
4478	4478	0.65 est.	--	--	--	--	--	--			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	---	---	---	---	---	---	1036	45	1036	45	171 hr.
1.	3/4" choke			100	--	62	100		560		3 hr.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcid
1	11.00	--	112	.9981	1.240	1.000	1525
2.							
3.							
4.							
5.							

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	Mc/ bbl.
1	.1671	522	1.392	0.973	A.P.I. Gravity of Liquid Hydrocarbons	Deq.
2.					Specific Gravity Separator Gas	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX
4.					Critical Pressure 670 P.S.I.A.	670 P.S.I.A.
5.					Critical Temperature 375 R	375 R

NO.	P _c	P _w	R _c ²	R _w ²	R _c ² - R _w ²	(1) $\frac{P_c^2}{R_c^2 - R_w^2} = 1.1377$	(2) $\left[\frac{R_c^2}{R_c^2 - R_w^2} \right]^n = 1.10159$
1	12,544	565	132,890	965,414			
2.							
3.							
4.							
5.							

$AOF = C \left[\frac{R_c^2}{R_c^2 - R_w^2} \right]^n = 1680$

Absolute Open Flow		1680		Mc/d @ 15.025		Angle of Slope		--		Slope, n		0.75			
Remarks:															
Approved By Commission:				Conducted By:				Calculated By:				Checked By:			
				W. E. Landry				W. E. Landry				W. E. Landry			