

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS-WELL

Form C-122
Revised 9-1-65

RECEIVED
FEB 20 1985
OIL DIV.
DIST 2

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 11-3-83		FEB 20 1985	
Company Dakota Resources, Inc.				Connection			
Pool Wildcat				Formation Dakota		Unit	
Completion Date 10-25-83		Total Depth 2660		Plug Back TD 2575		Elevation 7103 GL	
Csg. Size 4 1/2		Wt. 10.5		Set At 2635		Perforations: From 2416 To 2424	
Tng. Size 2 3/8		Wt. 4.7		Set At 23.95		Perforations: From 2428 To 2429	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None		Farm or Lease Name Santa Fe Pacific	
Producing Thru Tubing		Reservoir Temp. °F 6		Mean Annual Temp. °F		Baro. Press. - P _a	
L		H		Gg		State New Mexico	
				% CO ₂		% N ₂	
				% H ₂ S		Prover. Positive Choke	
						Meter Run	
						Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	2 x 6 x 3/4						776	60	780		
2.							97		192		3 hrs.
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	11.00		109	1.000	1.240	1.010	1502
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.G. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 792 P _c ² 627264				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0711$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0532$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²			
1.		204	41616	585648			
2.							
3.							
4.							
5.							

ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1582$			
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Absolute Open Flow 1582		Mcf @ 15.025	Angle of Slope 53.13	Slope, n .75
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Remarks:			
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Approved By Commission:	Conducted By: Richard Housh	Calculated By: Neil Tefteller	Checked By:
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