

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 07-14-82	
Company Robert L. Bayless				Connection Gas Company of New Mexico	
Pool Ballard Pic. Cliffs				Formation Pictured Cliffs	
Completion Date 07-06-82		Total Depth 2250 ft.		Plug Back TD 2214 ft.	
Elevation 6630 ft. GL		Farm or Lease Name AXI <i>Apache</i>			
Csq. Size 2.875	Wt. 6.5#	d 2.441	Set At 2235 ft.	Perforations: From 2065 To 2126	
Thq. Size 1.660	Wt. 2.4#	d 1.380	Set At 2040 ft.	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At none	
Producing Thru tubing		Reservoir Temp. °F #		Mean Annual Temp. °F	
Baro. Press. - P _a 12 psia (est.)		State New Mexico			
L	H	Gg .650	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run		Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	8 days						488		496		
1.	2 inch			36			36	60°	118		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		48	1.000	.9608	1.007	574
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 508		P _c ² 258064				
NO	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.07008}{}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.05925}{}$
1		130	16900	241164		
2						
3						
4						
5						

AOF = Q	$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{608}{}$
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$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 608$$

Absolute Open Flow 608 Mcfd @ 15.025 Angle of Slope θ Slope, n .85

Remarks:

Approved By Division	Conducted By: Kevin H. McCord	Calculated By: Kevin H. McCord	Checked By: Robert L. Bayless
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