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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

RECEIVED

Form C-122
Revised 4-1-91

JUN 7 1993

OIL CON. DIV.

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Dugan Production Corp.					Lease or Unit Name Hendrix				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-26-93		Well No. 1		
Completion Date 5-11-93		Total Depth 1535'		Plug Back TD 1500'		Elevation 6740' GL		Unit Ltr. - Sec. - TWP - Rge. B- 7- 22N- 8W	
Crg. Size 4 1/2"		Wt. 10.5#	d 4.052	Set At 1531'	Perforations: From: 1249 To: 1363		Country San Juan		
Tbg. Size 1 1/4"		Wt. 2.3#	d 1.380	Set At 1306'	Perforations: From: NA To:		Pool Wildcat		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single					Packer Set At NA		Formation Chacra		
Producing Thru tubing		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a 12		Connection	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	
		.62							

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI						240	65°	240	65°	7 days
1.										
2.										
3.	2" x 3/4"					8	65°	120		3 hrs
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\frac{h_w}{P_a}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.							
2.							
3.	11		20	.9952	1.29	1.00	282
4.							
5.							

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl
1.				1.000	A.P. I Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX
4.					Critical Pressure	P.S.I.A. P.S.I.A.
5.					Critical Temperature	R R

P_c 252 P_a 63,504

NO.	P _i ²	P _w	P _w ²	P _i ² - P _w ²
1.				
2.				
3.		132	17424	46080
4.				
5.				

1) $\frac{P_i^2}{P_i^2 - P_w^2} = 1.3781$ (2) $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 1.272$

AOF = Q $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 359$

Absolute Open Flow	359	Mcf/d @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks: light-medium spray water

Approved By Division	Conducted By: M. Brown	Calculated By: J. Alexander	Checked By:
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