

Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088



MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Dugan Production Corp.						Lease or Unit Name Goodman					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-11-95					
Completion Date 1-4-95						Well No. 2					
Total Depth 1340						Plug Back TD 1298					
Csg. Size 2-7/8"						Elevation 6632					
Wt. d 6.5						Unit Loc. - Sec. - TWP - Rge. L 23 22N 8W					
Set At 1340						County San Juan					
Tbg. Size 1-1/4"						From: 1108 To: 1220					
Wt. d 2.4						Set At 1100					
From: To:						Pool W/C Bisti Chacra Ext.					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single - gas						Packer Set At					
Producing Thru tubing						Baro. Press - P _a 12					
Reservoir Temp. °F						Mean Annual Temp. °F					
L H Gg % CO ₂ % N ₂ % H ₂ S Prover						Meter Run Taps					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.						285		285		7 days
2.										
3.	2" x 3/4"					1		20		3 hrs
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_a}$	Pressure P _a	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1.							
2.							
3.	11		13	1.000	1.29	1.000	184
4.							
5.							

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	
1.					Mcft/bbl	
2.					A.P. I. Gravity of Liquid Hydrocarbons	
3.					Specific Gravity Separator Gas	
4.					Specific Gravity Flowing Fluid	
5.					Critical Pressure	
					Critical Temperature	

NO.	P _i ²	P _a	P _w ²	P _i ² - P _w ²
1.				
2.				
3.		32	1024	87,184
4.				
5.				

1) $\frac{P_i^2}{P_i^2 - P_w^2} = 1.0117$

2) $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 1.01$

AOF = Q $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 186$

P_a 297 P_i² 88,208

Absolute Open Flow 186 Mcfd @ 15.025

Angle of Slope θ	Slope, n .85
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Remarks: very dry

Approved By Division	Conducted By: Hall	Calculated By: Alexander	Checked By:
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