Initial Deliverebility

## NEW MEXICO OIL CONSERVATION COMMISSION GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA EXCEPT BARKER DOMÉ STORAGE AREA)

Pool	South Black	<u> </u>	Formation	<u>Pietured</u>	CITES	County_	ATTIDA	
Purchasing Pi	ipeline <b>Pasific</b>	. Morthwest	<u> Pipeline C</u>	orporation	Date Test F	iled	6-25-57	
Operator	ertheast Produ	stion Corp.		**S**		Well No	11-11	
	Sec <b></b>	•		Pay Zone	From 30		2000	
	7 WT.						T. Perf.	•
	ough: Casing						Estimated	
	Test: From							
Meter Run Siz	e	Orif	ice Size		.Type Chart_	<del></del> -	Гуре Тарѕ	
			OBSERVI	ED DATA				
Flowing casing	pressure (Dwt)				_psig + 12 =		psiα	(0
lowing tubing	pressure (Dwt)		·		_psig + 12 =		psia	(1
Flowing meter p	ressure (Dwt)			<del> </del>	_psig + 12 =		psia	(0
	oressure (meter readi		surement taker	n: ,		•		
	t reading						•	(0
	chart reading (	) <sup>2</sup> x spring (			=_		psia	(0
Meter error (c) -			<b>±</b>		=		psi	(•
· ·	'lowing column to me							
	w through tubing: (a)				= _		psi	(f
<del>-</del>	ige static meter pres t average reading	•	nart):	393	_psig + 12 =	60	psia	
	chart average reading		sp. const.		parg + rz =		psia	(ç (ç
	ven day avge, meter				=-		psia	(\ (1
$P_{+} = (h) + (f)$			•		=	- 4	psia	(i
	shut-in pressure (D	·	998	psig + 12 =	101		Ü	
Wellhead tubing shut-in pressure (Dwt)			· · · · · · · · · · · · · · · · · · ·	998	_psig + 12 =	101		(1
$c_{c} = (j) \text{ or } (k) \text{ w}$	hichever well flowed	d through			=	101	psia	(1
C								
Flowing Temp.			°F + 46	0	=		•Abs	(r
	(Meter Run)		F + 46		=	30	•Abs	
Flowing Temp. (Pd = ½ Pc = ½ (	(Meter Run) 1) X				=		•Abs	(r , (r
Flowing Temp. (Pd = ½ Pc = ½ (	(Meter Run) 1) X	FLOV	V RATE CAL		=		Abs psia	(r , (r
Flowing Temp.  Pd = ½ Pc = ½ (  ) =	(Meter Run) 1) X	FLOV V(d) DELI 2 - Pd = 765	V RATE CAL	CULATION =			Abs psia	(r (z /da
Flowing Temp.  Pd = ½ Pc = ½ (  ) =	(Meter Run) (1)  (1)  (2)  (3)  (4)	FLOV V(d) DELI 2 - Pd = 765	V RATE CAL	CULATION  =  COLCULATION			Abs psia	(r (z /da
Flowing Temp.  Pd = ½ Pc = ½ (  ) =	(Meter Run) (1)  X  (P)  LRY	FLOV V(d) DELI 2 - Pd = 765	V RATE CAL	CULATION  =  COLCULATION	<b>10</b>		Abs psia MCF/	(r , (r ∕da
Flowing Temp. ( $P_{d} = \frac{1}{2} P_{c} = \frac{1}{2} ($ $P_{d} = \frac{1}{2} P_{c} = \frac{1}{2} ($ (integrated) $P_{d} = \frac{1}{2} P_{c} =$	(Meter Run) (1)  (2) (Meter Run) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	FLOV V(d) DELI 2 - Pd = 765	V RATE CAL	CULATION  = CALCULATI  1.14	10 North	19	Abs psia MCF/	(t , (t) ∕da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  = Q	(Meter Run) (1)  (2) (Meter Run) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	FLOV V(d) DELI 2 - Pd = 765	VERABILITY	CULATION	10 North	19 west Prod hillipt.R/	MCF/C	(t , (t) ∕da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  = Q	(Meter Run) (1)  (2) (Meter Run) (3) (Meter Run) (4) (Meter Ru	FLOV V(d) DELI 2 - Pd = 765	V RATE CAL	CULATION	Morth Ray P	19 west Prod hillipt.R/	Abs psia MCF/	(t , (t) ∕da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  = Q	(Meter Run) (1)  (2) (Meter Run) (2) (Meter Run) (2) (Meter Run) (3) (4) (4) (4) (4) (4) (4) (4) (4) (5) (6) (7) (5) (6) (7) (6) (7) (7) (8) (8) (8) (8) (8) (8) (8) (8) (8) (8	FLOV V(d) DELI 2 - Pd = 765	VERABILITY  O75  631  psia  Mcf/day  psia  psia	CULATION  CALCULATI  1.14  Company By Title Witnessed by	Morth Ray P Aost	19 west Prod hillipt.R/	MCF/C	(t , (t) ∕da
Flowing Temp.   Pd = ½ Pc = ½ (	(Meter Run) (1)  (Meter Run) (1)  (P) (P) (RY 1910 149 607 505	FLOV V(d) DELI 2 - Pd = 765	V RATE CAL	CULATION  CALCULATI  1.14  Company By Title Witnessed by	Morth Ray P	19 west Prod hillipt.R/	MCF/C	(t , (t) ∕da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  SUMMA  C =  w =  d =  This is date of	(Meter Run) (1)  (Percentage of the percentage of th	FLOV V(d) DELI 2 - Pd = 765	VERABILITY  O75  631  psia  Mcf/day  psia  psia	CULATION  CALCULATI  1.14  Company By Title Witnessed by	Morth Ray P Aost	19 west Prod hillipt.R/	MCF/C	(1 , (1 /da
Flowing Temp.   Pd = ½ Pc = ½ (	(Meter Run) (1)  (Percentage of the percentage of th	$ \frac{\text{FLOV}}{\text{V(c)}} $ $ \frac{\text{V(d)}}{\text{V(d)}} $ $ \frac{\text{DELI}}{\text{c} - P_{d}^{2}} = 765 $ $ \frac{\text{c} - P_{w}^{2}}{\text{c} - P_{w}^{2}} = \frac{651}{\text{c}} $	VERABILITY  O75  OS1  psia  Mcf/day  psia  psia  Mcf/day	CULATION	North Ray P Asst	19 west Prod hillipt.R/	MCF/C	(t , (t) ∕da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  SUMMA  C =  w =  d =  This is date of	(Meter Run) (1)  (Percentage of the percentage of th	$ \frac{\text{FLOV}}{\text{V(c)}} $ $ \frac{\text{V(d)}}{\text{V(d)}} $ $ \frac{\text{DELI}}{\text{c} - P_{d}^{2}} = 765 $ $ \frac{\text{c} - P_{w}^{2}}{\text{c} - P_{w}^{2}} = \frac{651}{\text{c}} $	VERABILITY  O75  SS1  psia  Mcf/day  psia  psia  Mcf/day  SCS OR FRICTION	COMPANY  COMPANY  By  Title  Witnessed by  Company  ON CALCULAT	Morth Ray P Aost	19 Lilling, R	MCF/C	(1 , (1 /da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  SUMMA  C =  w =  d =  This is date of	(Meter Run) (1)  (Percentage of the percentage of th	$ \frac{\text{FLOV}}{\text{V(c)}} $ $ \frac{\text{V(d)}}{\text{V(d)}} $ $ \frac{\text{DELI}}{\text{c} - P_{d}^{2}} = 765 $ $ \frac{\text{c} - P_{w}^{2}}{\text{c} - P_{w}^{2}} = \frac{651}{\text{c}} $	VERABILITY  O75  SS1  psia  Mcf/day  psia  psia  Mcf/day  SCS OR FRICTION	CULATION	North Ray P Asst	19 Lilling, R	MCF/o	(r , (r ∕da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  SUMMA  c =  w =  d =  This is date of Meter error con	(Meter Run) (1)  X  (Meter Run) (1)  X  (Meter Run) (1)  X  (P) (P) (P) (P) (P) (P) (P) (P) (P) (P	$ \frac{\text{FLOV}}{\text{V(c)}} $ $ \frac{\text{V(d)}}{\text{V(d)}} $ $ \frac{\text{DELI}}{\text{c} - P_d^2} = \frac{763}{651} $ $ \frac{\text{REMARF}}{\text{REMARF}} $	VERABILITY  O75  SS1  psia  Mcf/day  psia  psia  Mcf/day  SCS OR FRICTION	COMPANY  COMPANY  By  Title  Witnessed by  Company  ON CALCULAT	Morth Ray P Aost	= 19  west Fred hillipt.R	MCF/o	(r (r /da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  SUMMA  c =  w =  d =  This is date of Meter error con	(Meter Run) (1)  X  (Meter Run) (1)  X  (Meter Run) (1)  X  (P) (P) (P) (P) (P) (P) (P) (P) (P) (P	$ \frac{\text{FLOV}}{\text{V(c)}} $ $ \frac{\text{V(d)}}{\text{V(d)}} $ $ \frac{\text{DELI}}{\text{c} - P_d^2} = \frac{763}{651} $ $ \frac{\text{REMARF}}{\text{REMARF}} $	VERABILITY  O75  SS1  psia  Mcf/day  psia  psia  Mcf/day  SCS OR FRICTION	CULATION	Morth Ray P Aost	= 19  west Fred hillipt.R	MCF/o	(r (r /da
Flowing Temp.  Pd = ½ Pc = ½ (  integrated)  SUMMA  c =  w =  d =  This is date of Meter error con	(Meter Run) (1)  X  (Meter Run) (1)  X  (Meter Run) (1)  X  (P) (P) (P) (P) (P) (P) (P) (P) (P) (P	$ \frac{\text{FLOV}}{\text{V(c)}} $ $ \frac{\text{V(d)}}{\text{V(d)}} $ $ \frac{\text{DELI}}{\text{c} - P_d^2} = \frac{763}{651} $ $ \frac{\text{REMARF}}{\text{REMARF}} $	VERABILITY  O75  SS1  psia  Mcf/day  psia  psia  Mcf/day  SCS OR FRICTION	CULATION	Morth Ray P Aost	= 19  west Fred hillipt.R	MCF/o	(r (r /da