

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 12/3/69		DEC 4 1969 OIL CON COM. DIST. 3			
Company SOUTHERN UNION PRODUCTION CO. SOUTHERN UNION GAS COMPANY				Connection					
Pool BASIN				Formation DAKOTA					
Completion Date 11/22/69		Total Depth 7540		Plug Back TD 7426		Elevation 6645		Farm or Lease Name JICARILLA "K"	
Csg. Size 7.625	Wt. 26.40	d 6.969	Set At 3200	Perforations: From 7186 To 7408		Well No. 11			
Tbg. Size 4.500	Wt. 10.50	d 4.052	Set At 7456	Perforations: From 7309 To 7317		Unit Sec. Twp. Rge. E 2 25N 5W			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At		County RIO ARRIBA			
Producing Thru TUBING		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _g 12		State NEW MEXICO	
L 7305	H	Gg .700	% CO ₂	% N ₂	% H ₂ S	Prover		Meter Run	Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	2"		3/4"				2397		2354		7 DAYS
1.							210	60°	692		3 HOURS
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		222	1.0000	0.9258	1.026	2,607
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 2409	P _c ² 5,803,281	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.0934}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.0692}$	
NO.	P _t ²	P _w	R _w ²	P _c ² - R _w ²	
1		704	495,616	5,307,665	
2.					
3.					
4.					
5.					

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{2,787}$			
Absolute Open Flow 2,787		Mcf/d @ 15.025	Angle of Slope @ _____ Slope, n 0.75
Remarks: _____			

Approved By Commission:	Conducted By: KENNETH E. RODDY	Calculated By: KENNETH E. RODDY	Checked By: KENNETH E. RODDY
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