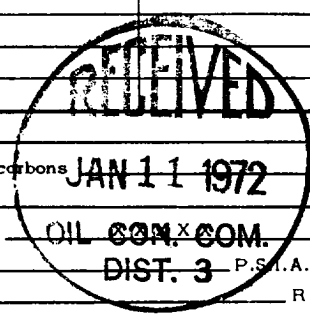


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 1/7/72																																																																																															
Company Southern Union Production Co.				Connection El Paso Natural Gas Company																																																																																															
Pool Basin				Formation Dakota																																																																																															
Completion Date 12/22/71		Total Depth 7210		Plug Back TD 7173																																																																																															
				Elevation 6752 GL																																																																																															
Farm or Lease Name Jicarilla "L"																																																																																																			
Csg. Size 5.500	Wt. 15.50	d 4.950	Set At 7209	Perforations: From 7084 To 7156																																																																																															
Well No. 6																																																																																																			
Tbg. Size 2.0625	Wt. 3.25	d 1.750	Set At	Perforations: From 7062 To 7070																																																																																															
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual - Gas - Oil				Packer Set At 6900																																																																																															
Producing Thru Tubing		Reservoir Temp. °F @		Baro. Press. - P _a 12																																																																																															
		Mean Annual Temp. °F		County Rio Arriba																																																																																															
L 7052		H	G _g 0.700	% CO ₂	% N ₂																																																																																														
				% H ₂ S	Prover																																																																																														
					Meter Run Taps																																																																																														
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="6">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td>2"</td> <td></td> <td>3/4"</td> <td></td> <td></td> <td></td> <td>2022</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>1.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>295</td> <td>63°</td> <td></td> <td></td> <td>7 Days</td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3 Hours</td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>						FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI	2"		3/4"				2022					1.							295	63°			7 Days	2.											3 Hours	3.												4.												5.											
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RATE OF FLOW CALCULATIONS																																																																																																			
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd																																																																																												
1	12.3650		307	0.9971	0.9258	1.036	3630																																																																																												
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NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio			Mcf/bbl.																																																																																											
1					A.P.I. Gravity of Liquid Hydrocarbons			Deg.																																																																																											
2.					Specific Gravity Separator Gas			X X X X X X X X																																																																																											
3.					Specific Gravity Flowing Fluid			OIL CON. COM.																																																																																											
4.					Critical Pressure			DIST. 3 P.S.I.A.																																																																																											
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P_c 2034 P_c² 4,137,156 <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_t²</th> <th>P_w²</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> <tr> <td>1</td> <td></td> <td></td> <td>791,739</td> <td>3,345,417</td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> </tr> </table> (1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2367$ AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4257$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1727$											NO.	P _t ²	P _w ²	P _w ²	P _c ² - P _w ²	1			791,739	3,345,417	2.					3.					4.					5.																																																															
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5.																																																																																																			
Absolute Open Flow 4257					Mcf @ 15.025		Angle of Slope °		Slope, n 0.75																																																																																										
Remarks:																																																																																																			
Approved By Commission:			Conducted By: Kenneth E. Roddy			Calculated By: Kenneth E. Roddy			Checked By: Kenneth E. Roddy																																																																																										