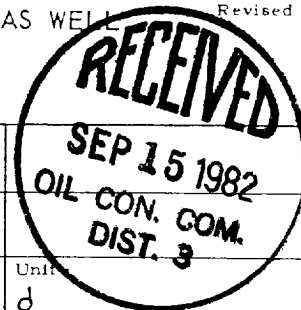


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Form C-122
Revised 9-1-65



Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9/14/82				
Company Conoco Inc.					Connection New				
Pool Ballard					Formation Picture Cliff				
Completion Date 9/2/82			Total Depth 2560		Plug Back TD 2529		Elevation 6684		Farm or Lease Name N.E. Haynes
Csg. Size 3 1/2	Wt. 9.3 #	d 2.992	Set At 2560	Perforations: From 2381 To 2435				Well No. 14	
Thg. Size None	Wt.	d	Set At	Perforations: From To				Unit Sec. Twp. Rge. D 22 24n. 5w	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas					Packer Set At None			County Rio Arriba	
Producing Thru Casing		Reservoir Temp. °F 94° @ 2402		Mean Annual Temp. °F 55°		Baro. Press. - P _a 12.2		State N.M.	
L 2402	H 2402	Gg .640	% CO ₂	% N ₂	% H ₂ S	Prover 3/4" C.N.	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow		
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F	
SI	7 DAYS									612 ±		S.I.
1.	3/4" x 6" Choke Nipple									97 ±	67°	3 hours
2.												
3.												
4.												
5.												

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		109.2	.9933	1.250	n/a.	1491.4
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.			
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
2.					Specific Gravity Separator Gas _____ X X X X X X X X			
3.					Specific Gravity Flowing Fluid _____ X X X X X			
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.			
5.					Critical Temperature _____ R _____ R			

$P_c = 2540 - P_c^2 = 2540 - 25.64$				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1				2540 - 25.73 = 2514.27
2.				
3.				
4.				
5.				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.006$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.005$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1498.85$

Absolute Open Flow	1498.85	Mcfd @ 15.025	Angle of Slope θ	Slope, n .85
Remarks:				

Approved By Commission:	Conducted By: R.A. Farmer	Calculated By: R.A. Farmer	Checked By:
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