

NEW MEXICO OIL CONSERVATION COMMISSION  
GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA  
EXCEPT BARKER DOME STORAGE AREA)

Pool Tapicito Formation Pictured Cliffs County Rio Arriba  
Purchasing Pipeline Southern Union Gas Company Date Test Filed 4-20-56  
Operator Southern Union Gas Company Lease Jicarilla Well No. 1-B  
Unit D Sec. 32 Twp. 26N Rge. 3W Pay Zone: From 3844 To 3818  
Casing: OD 7" WT. 20# Set At 3801' Tubing: OD 2 3/8" WT. 4.7# T. Perf. 3805'  
Produced Through: Casing    Tubing I Gas Gravity: Measured .655 Estimated     
Date of Flow Test: From 3/31/56 To 4/8/56 \* Date S.I.P. Measured 6-17-55  
Meter Run Size 4" Orifice Size 3/4" Type Chart Normal Type Taps Flange

OBSERVED DATA

Flowing casing pressure (Dwt)    psig + 12 =    psia (a)  
Flowing tubing pressure (Dwt)    psig + 12 =    psia (b)  
Flowing meter pressure (Dwt)    psig + 12 =    psia (c)  
Flowing meter pressure (meter reading when Dwt. measurement taken:  
Normal chart reading    psig + 12 =    psia (d)  
Square root chart reading (    )<sup>2</sup> x spring constant    =    psia (d)  
Meter error (c) - (d) or (d) - (c)    ±    =    psi (e)  
Friction loss, Flowing column to meter:  
(b) - (c) Flow through tubing: (a) - (c) Flow through casing    =    psi (f)  
Seven day average static meter pressure (from meter chart):  
Normal chart average reading 484 psig + 12 = 496 psia (g)  
Square root chart average reading (    )<sup>2</sup> x sp. const.    =    psia (g)  
Corrected seven day avge. meter press. (p<sub>f</sub>) (g) + (e)    = 496 psia (h)  
P<sub>t</sub> = (h) + (f)    = 496 psia (i)  
Wellhead casing shut-in pressure (Dwt) 1,063 psig + 12 = 1,075 psia (j)  
Wellhead tubing shut-in pressure (Dwt) 1,060 psig + 12 = 1,072 psia (k)  
P<sub>c</sub> = (j) or (k) whichever well flowed through    = 1,072 psia (l)  
Flowing Temp. (Meter Run) 65 °F + 460    = 525 °Abs (m)  
P<sub>d</sub> = 1/2 P<sub>c</sub> = 1/2 (l)    = 536 psia (n)

FLOW RATE CALCULATION

Q = 300 X  $\left( \frac{\sqrt{(c)}}{\sqrt{(d)}} \right)^*$  = 300 MCF/day  
(Integrated)

DELIVERABILITY CALCULATION

D = Q 300  $\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n$  0.85 9.557 96102 = 288 MCF/day.  
861,888 903,168 901,848 9622

SUMMARY

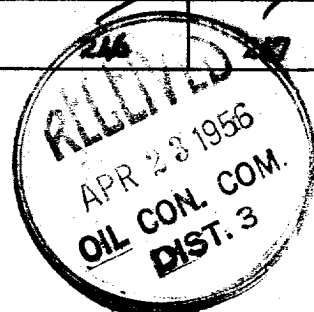
P<sub>c</sub> = 1072 psia  
Q = 300 Mcf/day  
P<sub>w</sub> = 497 psia  
P<sub>d</sub> = 536 psia  
D = 288 MCF/day

Company Southern Union Gas Company  
By L. S. Muenchink  
Title Jr. Petroleum Engineer  
Witnessed by     
Company   

\* This is date of test  
\* Meter error correction factor

REMARKS OR FRICTION CALCULATIONS

|      | $\left( \frac{F_c Q}{1.27 \times 10^{-3}} \right)^2$ | $(1 - e^{-8})$ | P <sub>t</sub> <sup>2</sup> | P <sub>t</sub> <sup>2</sup> + R <sup>2</sup> | P <sub>w</sub> |
|------|------------------------------------------------------|----------------|-----------------------------|----------------------------------------------|----------------|
|      | (F <sub>c</sub> Q) <sup>2</sup>                      | R <sup>2</sup> | (Column i)                  |                                              |                |
| 2492 | 7.95                                                 | 1.320          | 246                         | 497                                          | 496            |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |
|      |                                                      |                |                             |                                              |                |



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