

NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Basin Dakota Formation Dakota County Rio Arriba
 Initial Yes Annual _____ Special _____ Date of Test 1-17-62
 Company Caulkins Oil Company Lease Breach "E" Well No. D-50
 Unit A Sec. 5 Twp. 26 N Rge. 6 W Purchaser El Paso Natural Gas Company
 Casing 4 1/2 Wt. 11.6 I.D. 4.00 Set at 7610 Perf. 7210 To 7432
 Tubing 2-3/8" Wt. 4.7 I.D. 1.995 Set at 7208 Perf. 7208 To _____
 Gas Pay: From 7210 To 7432 L 7208 xG .660 -GL 4757 Bar.Press. 12
 Producing Thru: Casing _____ Tubing Yes Type Well Single Gas
 Single-Bradenhead-G. G. or G.O. Dual
 Date of Completion: 12-24-62 Packer none Reservoir Temp. 185°

OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) Type Taps _____

| No. | Flow Data | | | | | Tubing Data | | Casing Data | | Duration of Flow Hr. |
|-----|----------------------|------------------------|-------------|----------------------|-----------|-------------|-----------|-------------|-----------|----------------------|
| | (Prover) (Line) Size | (Choke) (Orifice) Size | Press. psig | Diff. h _w | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. | |
| SI | | | | | | 2275 | | 2280 | | SI 7 days |
| 1. | | 3/4" | | | | 355 | | 1182 | | 3 hours |
| 2. | | | | | | | | | | |
| 3. | | | | | | | | | | |
| 4. | | | | | | | | | | |
| 5. | | | | | | | | | | |

FLOW CALCULATIONS

| No. | Coefficient (24-Hour) | $\sqrt{h_w p_f}$ | Pressure psia | Flow Temp. Factor Ft | Gravity Factor F _g | Compress. Factor F _{pv} | Rate of Flow Q-MCFPD @ 15.025 psia |
|-----|-----------------------|------------------|---------------|----------------------|-------------------------------|----------------------------------|------------------------------------|
| 1. | 14.1605 | | 367 | 1.0048 | .9535 | 1.041 | 5175 |
| 2. | | | | | | | |
| 3. | | | | | | | |
| 4. | | | | | | | |
| 5. | | | | | | | |

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio _____ cf/bbl.
 Gravity of Liquid Hydrocarbons _____ deg.
 P_c _____ (1-e^{-S})
 Specific Gravity Separator Gas _____
 Specific Gravity Flowing Fluid _____
 P_c 2292 P_c² 5,253,264

| No. | P _w P _t (psia) | P _t ² | F _c Q | (F _c Q) ² | (F _c Q) ² (1-e ^{-S}) | P _w ² | P _c ² -P _w ² | Cal. P _w | P _w /P _c |
|-----|--------------------------------------|-----------------------------|------------------|---------------------------------|------------------------------------------------------|-----------------------------|----------------------------------------------------------|---------------------|--------------------------------|
| 1. | | | | | | 1,425,636 | 3,827,628 | | 520 |
| 2. | | | | | | | | | |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

Absolute Potential: 6553 MCFPD; n 91.37ⁿ 1.2662

COMPANY Caulkins Oil Company
 ADDRESS Box 780, Farmington, New Mexico
 AGENT and TITLE Superintendent
 WITNESSED _____
 COMPANY _____

REMARKS

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia
- P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if
flowing through casing.) psia
- P_f = Meter pressure, psia.
- h_w = Differential meter pressure, inches water.
- F_g = Gravity correction factor.
- F_t = Flowing temperature correction factor.
- F_{pv} = Supercompressability factor.
- n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .