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NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122  
Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Tapacito Formation Pictured Cliffs County Rio Arriba  
Initial X Annual          Special          Date of Test 12-20-57  
Company Northwest Production Corp. Lease "N" Well No. 11-7  
Unit D Sec. 7 Twp. 26N Rge. 4W Purchaser Not connected  
Casing 5-1/2 Wt. 18.5 I.D.          Set at 3886 Perf. XXXX 3788 To 3841  
Tubing 1-1/4 Wt. 2.3 I.D.          Set at 3788 Perf.          To           
Gas Pay: From 3788 To 3841 L          est. xG .650 -GL          Bar.Press.           
Producing Thru: Casing          Tubing X Type Well Single  
Date of Completion: 12-13-57 Packer No Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp.         

OBSERVED DATA

Tested Through (Prover) (Choke) (Prover) Type Taps         

| No. | Flow Data                  |  |                |                         |              | Tubing Data    |              | Casing Data    |              | Duration<br>of Flow<br>Hr. |
|-----|----------------------------|--|----------------|-------------------------|--------------|----------------|--------------|----------------|--------------|----------------------------|
|     | (Prover)<br>(Line)<br>Size | (Choke)<br>( <del>Prover</del> )<br>Size | Press.<br>psig | Diff.<br>h <sub>w</sub> | Temp.<br>°F. | Press.<br>psig | Temp.<br>°F. | Press.<br>psig | Temp.<br>°F. |                            |
| SI  |                            |  |                |                         |              | 1032           |              | 1033           |              | SI                         |
| 1.  |                            |  |                |                         |              |                |              |                |              |                            |
| 2.  |                            |  |                |                         |              |                |              |                |              |                            |
| 3.  |                            | 3/4                                      |                |                         |              | 41             | 51           | 397            |              | 3 hrs                      |
| 4.  |                            |  |                |                         |              |                |              |                |              |                            |
| 5.  |                            |  |                |                         |              |                |              |                |              |                            |

FLOW CALCULATIONS

| No. | Coefficient<br>(24-Hour) | $\sqrt{h_w P_f}$ | Pressure<br>psia | Flow Temp.<br>Factor<br>F <sub>t</sub> | Gravity<br>Factor<br>F <sub>g</sub> | Compress.<br>Factor<br>F <sub>pv</sub> | Rate of Flow<br>Q-MCFPD<br>@ 15.025 psia |
|-----|--------------------------|------------------|------------------|--|-------------------------------------|--|--|
| 1.  |                          |                  |                  |  |                                     |  |  |
| 2.  |                          |                  |                  |  |                                     |  |  |
| 3.  | 12.3850                  |                  | 53               | 1.0008                                 | .9808                               | 1.011                                  | 642                                      |
| 4.  |                          |                  |                  |  |                                     |  |  |
| 5.  |                          |                  |                  |  |                                     |  |  |

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio          cf/bbl.  
Gravity of Liquid Hydrocarbons          deg.  
F<sub>c</sub>          (1-e<sup>-S</sup>)  
Specific Gravity Separator Gas           
Specific Gravity Flowing Fluid           
P<sub>c</sub> 1045 P<sub>c</sub><sup>2</sup> 1092.0

| No. | P <sub>w</sub><br>P <sub>t</sub> (psia) | P <sub>t</sub> <sup>2</sup> | F <sub>c</sub> Q | (F <sub>c</sub> Q) <sup>2</sup> | (F <sub>c</sub> Q) <sup>2</sup><br>(1-e <sup>-S</sup> ) | P <sub>w</sub> <sup>2</sup> | P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup> | Cal.<br>P <sub>w</sub> | P <sub>w</sub><br>P <sub>c</sub> |
|-----|---|-----------------------------|------------------|---------------------------------|---|-----------------------------|--|------------------------|----------------------------------|
| 1.  |   |                             |                  |                                 |   |                             |  |                        |                                  |
| 2.  |   |                             |                  |                                 |   |                             |  |                        |                                  |
| 3.  | 409                                     |                             |                  |                                 |   | 167.3                       | 924.7  |                        | 1.181                            |
| 4.  |   |                             |                  |                                 |   |                             |  |                        |                                  |
| 5.  |   |                             |                  |                                 |   |                             |  |                        |                                  |

Absolute Potential: 739 MCFPD; n XXXXXXXX .85/1.15183  
COMPANY Northwest Production Corporation  
ADDRESS 204 North Orchard, Farmington, New Mexico  
AGENT and TITLE L. E. Gilbert, Asst. Dir. Engr.  
WITNESSED           
COMPANY         

REMARKS



## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .

## DRILLING DEPARTMENT

COMPANY **Northwest Production Corp.**

LEASE "N" WELL NO. 11-7

DATE OF TEST      **Dec. 20, 1957**

SHUT IN PRESSURE (PSIG): TUBING 1032 CASING 1033 S. I. PERIOD 7 DAYS

SIZE BLOW NIPPLE \_\_\_\_\_

FLOW THROUGH      **3/4" T.C. Choke**      WORKING PRESSURES FROM      **Casing**

[illegible]

START AT: 11:10 AM END TEST AT 2:10 PM

REMARKS: \_\_\_\_\_

TESTED BY: **L. E. Gilbert**

WITNESS:

|                                    |                          |   |
|------------------------------------|--------------------------|---|
| <b>OIL CONSERVATION COMMISSION</b> |                          |   |
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