

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

C O R R E C T E D T E S T

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 7/8/68	
Company SOUTHERN UNION PRODUCTION CO.				Connection SOUTHERN UNION GAS COMPANY		
Pool BLANCO				Formation MESAVERDE		Unit
Completion Date 6/15/68		Total Depth 8036		Plug Back TD 8020		Elevation 6933
Farm or Lease Name JICARILLA "A"						Well No. 9
Csg. Size 7.625	Wt. 26.40	d 6.969	Set At 3705	Perforations: From 5714 To 5826		Unit Sec. Twp. Rge. C 14 26N 4W
Thd. Size 1.900	Wt. 2.75	d 1.610	Set At 5800	Perforations: From 5792 To 5800		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple DUAL - GAS - GAS					Packer Set At 7660	
Producing Thru TUBING		Reservoir Temp. °F @		Mean Annual Temp. °F 12		County RIO ARriba
Baro. Press. - P _a 12		State NEW MEXICO				
L 5780	H	Gg .700	% CO ₂	% N ₂	% H ₂ S	Prover
Meter Run		Taps				

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	2"		3/4"				1137		1132		7 DAYS
1.							205	52°	786		3 HOURS
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		217	1.0078	.9258	1.027	2571
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbon	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature	Mcf/bbl.	Deg.
1.												
2.												
3.												
4.												
5.												

P _c 1149	P _c ² 1,320,201				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	
1		798	636,804	683,397	
2					
3					
4					
5					

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.9318}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{4,213}$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.6386}$

Absolute Open Flow 4213	Mcf/d @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks: _____

Approved By Commission:	Conducted By: KENNETH E. RODDY	Calculated By: KENNETH E. RODDY	Checked By: KENNETH E. RODDY
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2							
3							
4							
5							

NO.	P _r	Temp. °R	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1			A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2			Specific Gravity Separator Gas _____
3			Specific Gravity Flowing Fluid _____
4			Critical Pressure _____ P.S.I.A.
5			Critical Temperature _____ R

P _c 1144	P _c ² 1,308,736	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.9477}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.6487}$
NO.	P _t ²	P _w	P _w ²
1		798	636,804
2			
3			
4			
5			

Absolute Open Flow 4,239 Mcfd @ 15.025		Angle of Slope θ _____	Slope, n .75
Remarks: _____			
Approved By Commission:	Conducted By: KENNETH E. RODDY	Calculated By: KENNETH E. RODDY	Checked By: KENNETH E. RODDY