

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

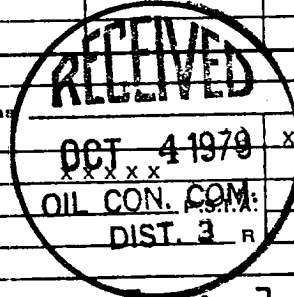
Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 10-1-79	
Company Southland Royalty Company		Connection Gas Company of New Mexico	
Pool Blanco		Formation Pictured Cliffs	
Completion Date 9-24-79		Total Depth 6215'	Plug Back TD 6120'
Elevation 7072' GR		Farm or Lease Name Jicarilla 101	
Csg. Size 7.000 4.500	Wt. 20# 10.50#	d 6.456 4.052	Set At 4092' 3934-6215'
Perforations: From 3796' To 3841'		Well No. #8	
Tbg. Size 1.900	Wt. 2.76#	d 1.610	Set At 3839
Perforations: From --- To ---		Unit Sec. Twp. Rye. N 12 26N 4W	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G. G. Multiple		Packer Set At 4040'	
Producing Thru Tbg		Reservoir Temp. °F @	Mean Annual Temp. °F 12.2
Baro. Press. - P _a 12.2		State New Mexico	
L	H	G _g .700	% CO ₂
		% N ₂	% H ₂ S
Prover		Meter Run	Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							970		1010	
1.	2"		3/4"				95		475	
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		107.2	1.0000	.9258	1.0000	1227
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____
3.					Specific Gravity Flowing Fluid _____
4.					Critical Pressure _____ P.S.I.A.
5.					Critical Temperature _____ R



$P_c = 1022.2$ $P_c^2 = 1,044,893$	$(1) \frac{P_c^2}{P_c^2 - R_w^2} = 1.2939$	$(2) \left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.2449$																														
<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>NO.</th> <th>P_t²</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> </thead> <tbody> <tr> <td>1</td> <td></td> <td>487.2</td> <td>237,364</td> <td>807,529</td> </tr> <tr> <td>2</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table>	NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	1		487.2	237,364	807,529	2					3					4					5					$AOF = Q \left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1527$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²																												
1		487.2	237,364	807,529																												
2																																
3																																
4																																
5																																

Absolute Open Flow	1527	Mcf/d @ 15.025	Angle of Slope θ	Slope, n .85
--------------------	------	----------------	------------------	--------------

Remarks:			
Approved By Commission:	Conducted By: Dwayne Horton	Calculated By: James Smith	Checked By: