

OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENTP. O. BOX 2088
SANTA FE, NEW MEXICO 87501Form C-122
Revised 10-1-78

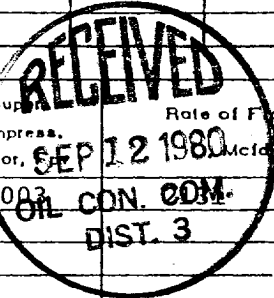
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 9/10/80	
Company J. Gregory Merrion			Connection New Well		
Pool Ballard Pictured Cliffs			Formation Pictured Cliffs		Unit
Completion Date 8/26/80		Total Depth 2650	Plug Back TD 2620'		Elevation 6605'
Casing Size 2.875"		Wt. 6.5#	d 2.441	Set At 2636'	Perforations: From 2408 To 2556
Tub. Size none		Wt.	d	Set At	Perforations: From To
Type Well - Single - Brdenhead - G.G. or G.O. Multiple Tubingless completion				Packer Set At none	
Producing Thru Casing		Reservoir Temp. *F #	Mean Annual Temp. *F		Baro. Press. - P _a 12.0
L		H	G _g .650	% CO ₂	% N ₂
				% H ₂ S	Prover 2"
					Meter Run
					Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI									605		SIP
1.	2" x 1-1/4"			50		60 ⁰			50		3 hr.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Supp. Rate of Flow Compress. Factor, F _c
1	27.63		62	1.000	1.240	1.003
2.						
3.						
4.						
5.						



NO.	P _t	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas	XXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXX
4.					Critical Pressure	P.S.I.A.
5.					Critical Temperature	R

P _c 617		P _c ² 380689			(1) $\frac{P_c^2}{P_t^2 - P_w^2} = \frac{1.0102}{}$		(2) $\left[\frac{P_c^2}{P_t^2 - P_w^2}\right]^n = \frac{1.0087}{}$	
NO	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_t^2}{P_t^2 - P_w^2}\right]^n = \frac{2149}{}$			
1		62	3844	376845				
2								
3								
4								
5								

$$AOF = 0 \left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 2149$$

Absolute Open Flow	2149	Mcf @ 15.025	Angle of Slope	Slope, n .85
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Remarks: Well produced dry gas throughout test.

Approved By Division	Conducted By: John C. Anderson	Calculated By: John C. Anderson	Checked By: Steven S. Dunn, Engineer
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