

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input checked="" type="checkbox"/> Special		Test Date 6-4-81									
Company Amoco Production Company		Connection Northwest Pipeline Corporation									
Pool Gonzales		Formation Mesaverde									
Completion Date 3-22-81		Total Depth 5300	Plug Back TD 5253								
		Elevation 6513									
Farm or Lease Name Jicarilla Contract 155											
Csg. Size 5.500	Wt. 14	d 5.012	Set At 5300								
Perforations: From 5014 To 5167		Well No. 27									
Thq. Size 2.063	Wt. 3.25	d 1.751	Set At 5184								
Perforations: From open To ended		Unit Sec. Twp. R1/4 J 32 26N 5W									
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual		Packer Set At 3880	County Rio Arriba								
Producing Thru Tubing	Reservoir Temp. °F @	Mean Annual Temp. °F	Baro. Press. - P _a								
State New Mexico											
L	H	G _g	% CO ₂ % N ₂ % H ₂ S								
Prover		Meter Run	Taps								
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	62 Days						799				
1.	2.375		.750				154				3 hrs
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{spv}	Rate of Flow Q, Mcfd				
1.	12.365		166	1.000	.9608	1.017	2006				
2.											
3.											
4.											
5.											
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.					
1.					A.P.I. Gravity of Liquid Hydrocarbons	Deg.					
2.					Specific Gravity Separator Gas	X X X X X X X X					
3.					Specific Gravity Flowing Fluid	X X X X X					
4.					Critical Pressure	P.S.I.A.					
5.					Critical Temperature	R					
P _c 811 P _c ² 657721											
NO.	P _f	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3641$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2622$					
1.		419	175561	482160							
2.											
3.											
4.											
5.											
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2532$											
Absolute Open Flow 2532 Mcfd @ 15.025				Angle of Slope @		Slope, n 75					
Remarks: Heavy oil flow											
Approved By Commission		Conducted By JJB		Calculated By J. J. Barnett		Checked By					

