

OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENTP. O. BOX 2088
SANTA FE, NEW MEXICO 87501Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 1-29-91		RECEIVED FEB 14 1991 OIL CON. DIV DIST. 3	
Company TEXACO INC.				Connection NOT CONNECTED			
Pool BLANCO				Formation MESA VERDE			
Completion Date 1-10-91		Total Depth 7550		Plug back TD 7510		Elevation 6691 KB	
Csq. Size 5.500		Wt. 14#		Set At 5.012		Perforations: From 4992 To 5352	
Thq. Size 2.0625		Wt. 3.25		Set At 1.751		Perforations: From open To ended	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple GAS; GAS MULTIPLE				Packer Set At 5407'		Well No. 3E	
Producing Thru TUBING		Reservoir Temp. °F •		Mean Annual Temp. °F		Baro. Press. - P _a 12.0	
L 5312		H 5312		C _g .710EST		% CO ₂ % N ₂ % H ₂ S	
						Prover 2.00x6x.750	
						Meter Run 750	
						Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							1102		1150	
1.	2.000x6x.750						194	60	569	
2.	2.000x6x.750						109	60	493	
3.	2.000x6x.750						88	60	451	
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	11.000		206	1.000	1.187	1.024	2754
2	11.000		121	1.000	1.187	1.014	1602
3	11.000		100	1.000	1.187	1.000	1306
4.							
5.							

NO.	R _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons 52 @60 _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1162	P _c ² 1350244	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1887$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1384$
NO	P _t ²	P _w	P _w ²
1			
2			
3	463	214369	1135875
4			
5			

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1487$

$AOF = Q$

Absolute Open Flow 1487 _____ Mcfd @ 15.025	Angle of Slope ϕ _____	Slope, n .75
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Remarks: Well produced 32 BBls load water and 3 Bls of compensate in 3 HRS

Approved By Division	Conducted By:	Calculated By:	Checked By:
		PAUL PERHOSM	