

RECEIVED

SEP 10 1985

OIL CON. DIV.
DIST. 3

Supplement to
APPLICATION FOR CLASSIFICATION AS

HARDSHIP GAS WELL

Kimbell Oil Company of Texas

Salazar Well No. 4-E

N $\frac{1}{2}$ section 34, T.25N., R.6W., N.M.P.M.

Rio Arriba County, New Mexico

Basin Dakota Pool

1. The applicant expects that total restriction of gas production from this well over an extended period of time will result in "underground waste" (as defined by the General Information Applicable to Hardship Gas Well Classification). This expectation is based on two points discussed below.

First, this well has produced a regular amount of water, which means that suppression of the gas flow will also suppress removal of this water from the wellbore. As shown in the Report prepared on 8-15-85, this could cause permanent "skin" damage to the formation face. The water production averaged 4.5 bbls/day or an average gas/water ratio of 2.17 bbls/MMCF. Regular production, which will prevent this water from accumulating in the wellbore, is indicated as the only preventative action against permanent formation damage.

Secondly, the wells in the surrounding area indicate that formation damage due to water accumulation may have occurred. Two of these wells have been abandoned and may have not produced their true potential due to water damage. These wells are the Farming E No. 3-E in D-2-24N-6W and the Salazar No. 4 in H-34-25N-6W. There are two wells in the south half of section 34 which may have suffered damage due to shut-in periods in the last 5 years. These wells are the Federal Wells No. 3 and 3-E. We will attempt to prove that these wells experienced lost productivity and potential recoverable reserves in the hearing. Their performance is documented on the enclosed Production Tables.

As discussed in the Engineering Report dated 8-15-85 (which calculated a minimum flow rate to prevent damage to this well), unless sufficient gas production and incumbent water production is allowed this water cannot be removed from the wellbore. The exposure to accumulated water could cause permanent formation damage and this would result in loss of gas reserves due to the reduction in permeability. Prolonged shut-in of this well could produce this result and it has already been shut-in since June 1985.

2. The well had not been damaged as of June based on the deliverability test. The potential problem of damage to this well cannot be solved by completion practices because it is just that--a "potential" problem and not an actual problem at this

time. Therefore, no mechanical operations are appropriate until such time as damage has actually occurred. The historical attempt to prevent the problem was full production of this well initially to remove excess frac water and formation water. This led to the overproduced status of the well. Also, El Paso Natural Gas Co. (the purchaser) was contacted when the well was shut-in to determine what preventative steps could be taken to alleviate the overproduction problem and also prevent the possibility of long-term damage to the formation by water accumulation due to lack of production. The result of those contacts was our Administrative Request in August, and upon subsequent discussions with the NMOCD staff in Santa Fe, the scheduling of the hearing and this application for temporary relief. Our motivation is to prevent damage, as being the best cure for formation damage. We seek a minimum flow rate to prevent damage and potential loss of reserves.

3. As illustrated by the attached production table and graph, initial production of this well was on May 12, 1984 and water production has varied from essentially 3.3 to 8.9 bbls/day with water ratios between 1.75 bbls/MMCF and 12.33 bbls/MMCF, with an average of 2.17 bbls/MMCF. This performance indicates that the water influx is a regular occurrence and only regular production of the gas will prevent any water accumulation. The Report dated 8-15-85 shows that gas production of about 13,550 MCF/month is required to prevent the pressure drop which would occur if the well were damaged.

4. Gas Reserves Lost:

Estimated Original Gas-In-Place:

Volumetric Calculation = 3.95 BCF

BHP/Z vs. Cumulative plot = 4.45 BCF

Recoverable Reserves (assume 85% recovery)

3.35 to 3.78 BCF

Preliminary decline curve projection:

1.8 BCF

Cumulative Recovered as of 6-85:

586,993 MCF

Both the materials balance and decline curve analysis are subject to error at this point, due to the limited production history and pressure tests available.

Lost reserves are not possible to determine at this point because the well has not suffered the pressure drop and erratic productivity loss resulting from damage. However using the radial flow equation developed in the 8-15-85 Engineering Report and setting the parameters to 1 (indicating no change) except

for q (flow-rate) and pressure drop, one can see that a pressure drop of 50 psi will result in a 75% drop in flowrate. If the portion of this drop due to skin damage equals 10 psi, the reduced flow due to damage would be 20%. Also, according to Allen and Roberts in Production Operations, Vol. 2, a loss of 50% of the producibility will occur with a 5-fold decrease in permeability at the well face due to damage. Thus the resultant loss of reserves could be large with formation and pressure alterations as outlined above. During the hearing we will attempt to show the amount of loss the adjacent wells may have experienced due to water accumulation.

5. The producibility of this well is shown by the attached deliverability tests of 1984 and 1985 and the Production Table and plot. The well has had an average production rate to date of 1947 MCF/day. At present we believe that production is necessary to maintain this potential flow rate and prevent irreversible loss due to damage. But currently available tests show that abnormal producibility decline has not yet occurred.
6. A plat of the area is attached and list of adjacent wells.
7. See attached Production Tables of adjacent wells.
8. This well is overproduced by 317,158 MCF, which is 11 times over its allowable.

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE

Form approved.
Budget Bureau No. 42-R866.5.

WELL COMPLETION OR RECOMPLETION REPORT AND LOG*

1a. TYPE OF WELL: OIL GAS WELL DRY Other _____b. TYPE OF COMPLETION: NEW WELL WORK OVER DEEPEN PLUG BACK DIFF. RESVR. Other _____

2. NAME OF OPERATOR: Curtis J. Little

3. ADDRESS OF OPERATOR: P.O. Box 1258
Farmington, NM 87499

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*

At surface 1630' FNL & 1460' FWL

At top prod. interval reported below

At total depth Same

API # - 30-039-23368

14. PERMIT NO. DATE ISSUED

15. DATE SPUNDED 16. DATE T.D. REACHED 17. DATE COMPL. (Ready to prod.) 18. ELEVATIONS (DP, RBD, RT, GR, ETC.)* 19. ELEV. Casinghead
1-16-84 1/27/84 2/21/84 6378' GR 6378'20. TOTAL DEPTH, MD & TVD 21. PLUG, BACK T.D., MD & TVD 22. IF MULTIPLE COMPL.,
HOW MANY? 23. INTERVALS DRILLED BY ROTARY TOOLS CABLE TOOLS
6753' 6717' → 0-6753'

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)

6422-6672 KB Dakota

25. TYPE ELECTRIC AND OTHER LOGS RUN
IES, GR-CNL-Density

26. Casing Record (Report all strings set in well)

CASING SIZE	WEIGHT, LB./FT.	DEPTH SET (MD)	HOLE SIZE	CEMENTING RECORDS	AMOUNT PULLED
8 5/8"	28	222 KB	12-1/4"	145 sx. (171 cuft.; slurry)	none
4 1/2"	11.6	6759	7-7/8"	DV Tool 4574, 600 sx. & Poz	(774 cuft.)

27. Liner Record

SIZE	TOP (MD)	BOTTOM (MD)	SACKS CEMENT*	SCREEN (MD)	SIZE	DEPTH SET (MD)	PACKER SET (MD)
					2-3/8	6548	

28. Perforation Record (Interval, size and number)

6632-72 KB, 21 holes, 0.33" dia. 24" apart.
6548-76 KB, 6514-28, 6432-36, 6422-26, 29 holes, 0.33" dia. 24" apart.

29. Production Record (Method, rate, pressure, etc.)

30. Production Method (Flowing, gas lift, pumping—size and type of pump)

31. Date First Production 2/21/84 Flowing

32. Acid, Shot, Fracture, Cement Squeeze, Etc.

33. Depth Interval (MD) Amount and Kind of Material Used

6632-72 Acidize 1200 gals. HCL, 41500 lbs. sd.,

62930 gal. gel, BDP 2450 psi, ATP 3200 psi, AIR

28 BPM, ISIP 2100 psi. 6576-6422 Acidize 1700 gal.

HCL, 60000 lbs. sd., 93780 gals. gel, BDP 1900 psi

34. Date Last Production 2/21/84

35. Production Rate (BBL/DAY) 36. Oil Gravity-API (Corr.)

37. Water Rate (BBL/DAY) 38. Gas Rate (MCF/DAY)

39. Oil-Oil Ratio 40. Gas-Oil Ratio

41. Water-Oil Ratio 42. Gas-Water Ratio

43. Oil Gravity-API (Corr.) 44. Gas Gravity-API (Corr.)

45. Water Gravity-API (Corr.) 46. Gas Gravity-API (Corr.)

47. Oil Gravity-API (Corr.) 48. Gas Gravity-API (Corr.)

49. Water Gravity-API (Corr.) 50. Gas Gravity-API (Corr.)

51. Oil Gravity-API (Corr.) 52. Gas Gravity-API (Corr.)

53. Water Gravity-API (Corr.) 54. Gas Gravity-API (Corr.)

55. Oil Gravity-API (Corr.) 56. Gas Gravity-API (Corr.)

57. Water Gravity-API (Corr.) 58. Gas Gravity-API (Corr.)

59. Oil Gravity-API (Corr.) 60. Gas Gravity-API (Corr.)

61. Water Gravity-API (Corr.) 62. Gas Gravity-API (Corr.)

63. Oil Gravity-API (Corr.) 64. Gas Gravity-API (Corr.)

65. Water Gravity-API (Corr.) 66. Gas Gravity-API (Corr.)

67. Oil Gravity-API (Corr.) 68. Gas Gravity-API (Corr.)

69. Water Gravity-API (Corr.) 70. Gas Gravity-API (Corr.)

71. Oil Gravity-API (Corr.) 72. Gas Gravity-API (Corr.)

73. Water Gravity-API (Corr.) 74. Gas Gravity-API (Corr.)

75. Oil Gravity-API (Corr.) 76. Gas Gravity-API (Corr.)

77. Water Gravity-API (Corr.) 78. Gas Gravity-API (Corr.)

80. Oil Gravity-API (Corr.) 81. Gas Gravity-API (Corr.)

83. Water Gravity-API (Corr.) 84. Gas Gravity-API (Corr.)

86. Oil Gravity-API (Corr.) 87. Gas Gravity-API (Corr.)

89. Water Gravity-API (Corr.) 90. Gas Gravity-API (Corr.)

92. Oil Gravity-API (Corr.) 93. Gas Gravity-API (Corr.)

95. Water Gravity-API (Corr.) 96. Gas Gravity-API (Corr.)

98. Oil Gravity-API (Corr.) 99. Gas Gravity-API (Corr.)

101. Water Gravity-API (Corr.) 102. Gas Gravity-API (Corr.)

104. Oil Gravity-API (Corr.) 105. Gas Gravity-API (Corr.)

107. Water Gravity-API (Corr.) 108. Gas Gravity-API (Corr.)

110. Oil Gravity-API (Corr.) 111. Gas Gravity-API (Corr.)

113. Water Gravity-API (Corr.) 114. Gas Gravity-API (Corr.)

116. Oil Gravity-API (Corr.) 117. Gas Gravity-API (Corr.)

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125. Water Gravity-API (Corr.) 126. Gas Gravity-API (Corr.)

128. Oil Gravity-API (Corr.) 129. Gas Gravity-API (Corr.)

131. Water Gravity-API (Corr.) 132. Gas Gravity-API (Corr.)

134. Oil Gravity-API (Corr.) 135. Gas Gravity-API (Corr.)

137. Water Gravity-API (Corr.) 138. Gas Gravity-API (Corr.)

140. Oil Gravity-API (Corr.) 141. Gas Gravity-API (Corr.)

143. Water Gravity-API (Corr.) 144. Gas Gravity-API (Corr.)

146. Oil Gravity-API (Corr.) 147. Gas Gravity-API (Corr.)

149. Water Gravity-API (Corr.) 150. Gas Gravity-API (Corr.)

152. Lease Designation and Serial No. SF-080136

154. If Indian, Allottee or Tribe Name Salazar

156. Unit Agreement Name

158. Farm or Lease Name Salazar

160. Well No. 4-E

162. Field and Pool, or Wildcat Basin Dakota

164. Sec., T., R., M., or Block and Survey Sec. 34-T25N-R6W

166. County or Parish Rio Arriba

168. State NM

170. War Directional Survey Made No

21. Was Well Cored No

23. Bonded No

25. Was Well Cored No

27. Was Well Cored No

29. Bonded No

31. Was Well Cored No

33. Bonded No

35. Was Well Cored No

37. Bonded No

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325. Bonded No

327. Was Well Cored No

329. Bonded No

331. Was Well Cored No

333. Bonded No

335. Was Well Cored No

337. Bonded No

339. Was Well Cored No

**UNITED STATES GOVERNMENT
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY**

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on Items 22 and 24, and 33, below regarding separate reports for separate completions. If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form; see Item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in Item 22, and in Item 24, show the producing interval, or intervals, top(s), bottom(s), and name(s) (if any), for only the interval reported in Item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Socia Cement": Submit supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

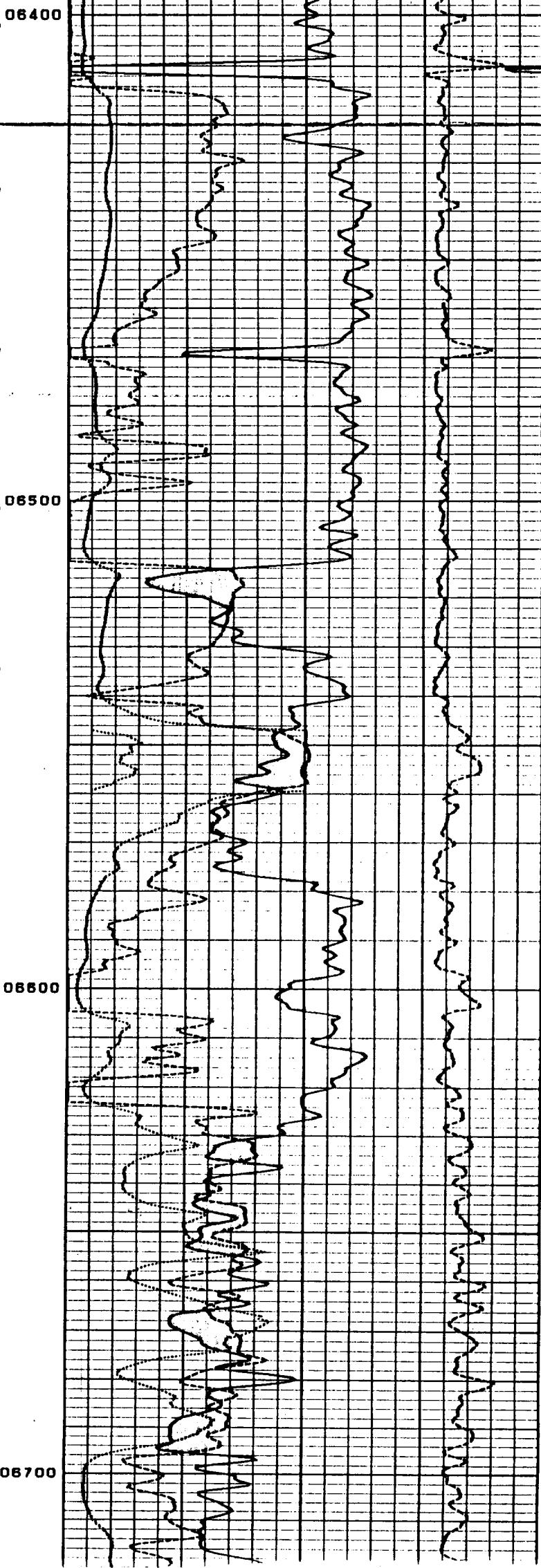
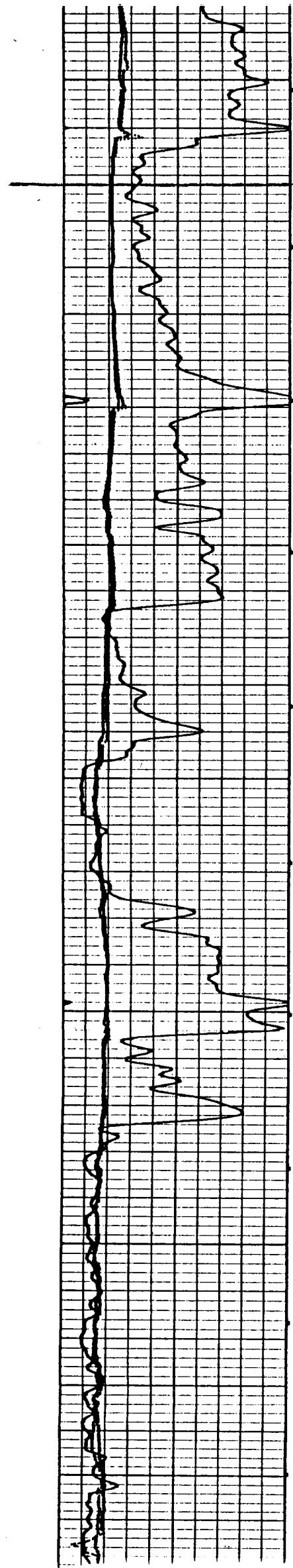
Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for Items 22 and 24 above.)

ST. SUMMARY OF POROUS ZONES: - KNOW ALL IMPORTANT ZONES OF POROSITY AND CONDUCTIVE CHANNELS: - CORED INTERVALS, AND ALL DEPTH-TEST, INCORPORATE, AND RECOVERIES

FORMATION	TOP	BOTTOM	DESCRIPTION, CONTENTS, ETC.	TESTS		
				TESTED	TESTED	TESTED
			Probably Water			
	1450	1522				
Ojo Alamo	1450					

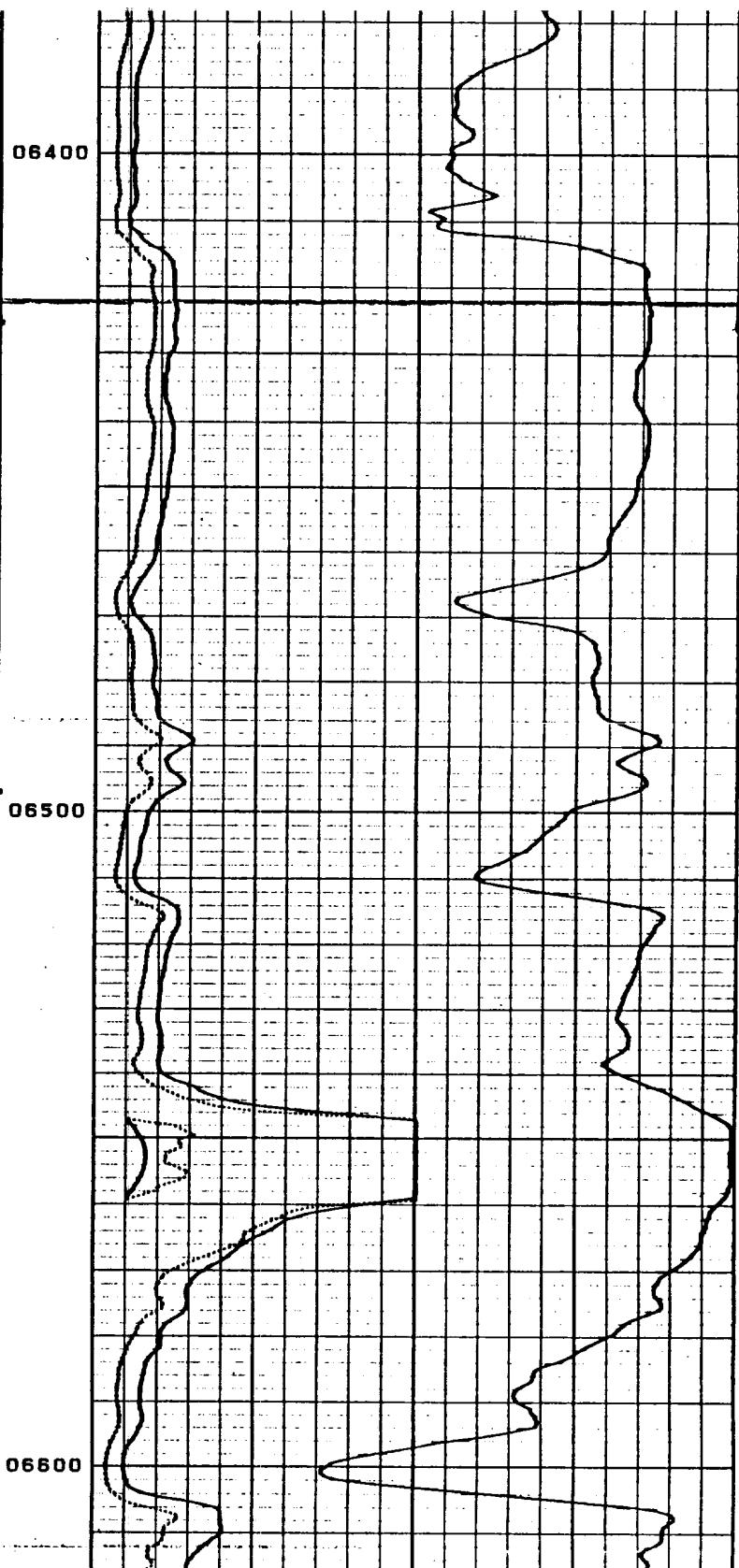
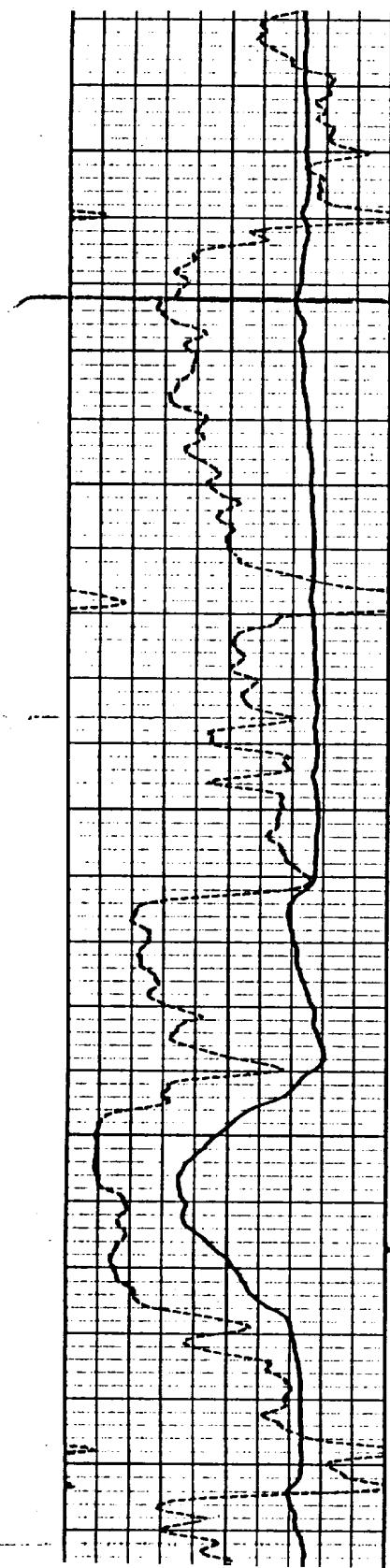
GEARHARTCOMPENSATED DENSITY
COMPENSATED NEUTRON
LOG

FILING NO.							
	COMPANY <u>CURTIS J. LITTLE</u>						
	WELL <u>SALAZAR NO.4-R</u>						
	FIELD <u>BASIN DAKOTA</u>						
	COUNTY <u>RIO ARRIBA</u>			STATE <u>NEW MEXICO</u>			
	LOCATION: <u>1630'FNL x 1460'FWL</u>					Other Services <u>IEL/GR</u>	
	SEC <u>34</u>	TWP <u>25N</u>	RGE <u>6W</u>				
Permanent Datum	<u>GROUND LEVEL</u>			Elev. <u>6378</u>	Elev.: <u>K.B. 6391</u>		
Log Measured from	<u>K.B.</u>			<u>13</u> Ft. Above Perm. Datum	D.F. <u>6390</u>		
Drilling Measured from	<u>K.B.</u>			G.L. <u>6378</u>			
Date	<u>1-27-84</u>						
Run No.	<u>ONE</u>						
Depth - Driller	<u>6753</u>						
Depth-Logger	<u>6753</u>						
Bottom logged interval	<u>6752</u>						
Top logged interval	<u>6150</u>						
Type fluid in hole	<u>GEL</u>						
Density	Visc.	<u>9.0</u>	<u>60</u>				
pH	Fluid Loss	<u>7.5</u>	<u>7</u>				
Max rec. temp., deg F.		<u>180</u>	<u>°F</u>		<u>°F</u>		<u>°F</u>
Source of Samples	<u>Mud Pit</u>						
Rm @ Meas. Temp.	<u>1.8 @ 74 °F</u>				<u>@ °F</u>	<u>@ °F</u>	<u>@ °F</u>
Rmf @ Meas. Temp.	<u>1.4 @ 69 °F</u>				<u>@ °F</u>	<u>@ °F</u>	<u>@ °F</u>
Rmc @ Meas. Temp.	<u>1.2 @ 68 °F</u>				<u>@ °F</u>	<u>@ °F</u>	<u>@ °F</u>
Source Rmf	Source Rmc	<u>M</u>	<u>M</u>				
Time	End Circulation	<u>20:00</u>					
	Logger on Bottom	<u>02:45</u>					
Recorded By	<u>Mease</u>						
Witnessed By	<u>Mr. Curtis Little</u>						
Run No.	Bore-Hole Record			Casing Record			
	Bit	From	To	Size	Wgt.	From	To
One	<u>12$\frac{1}{2}$</u>	<u>Surface</u>	<u>222</u>	<u>8 5/8</u>	<u>---</u>	<u>Surface</u>	<u>222</u>
One	<u>7 7/8</u>	<u>222</u>	<u>6753</u>				

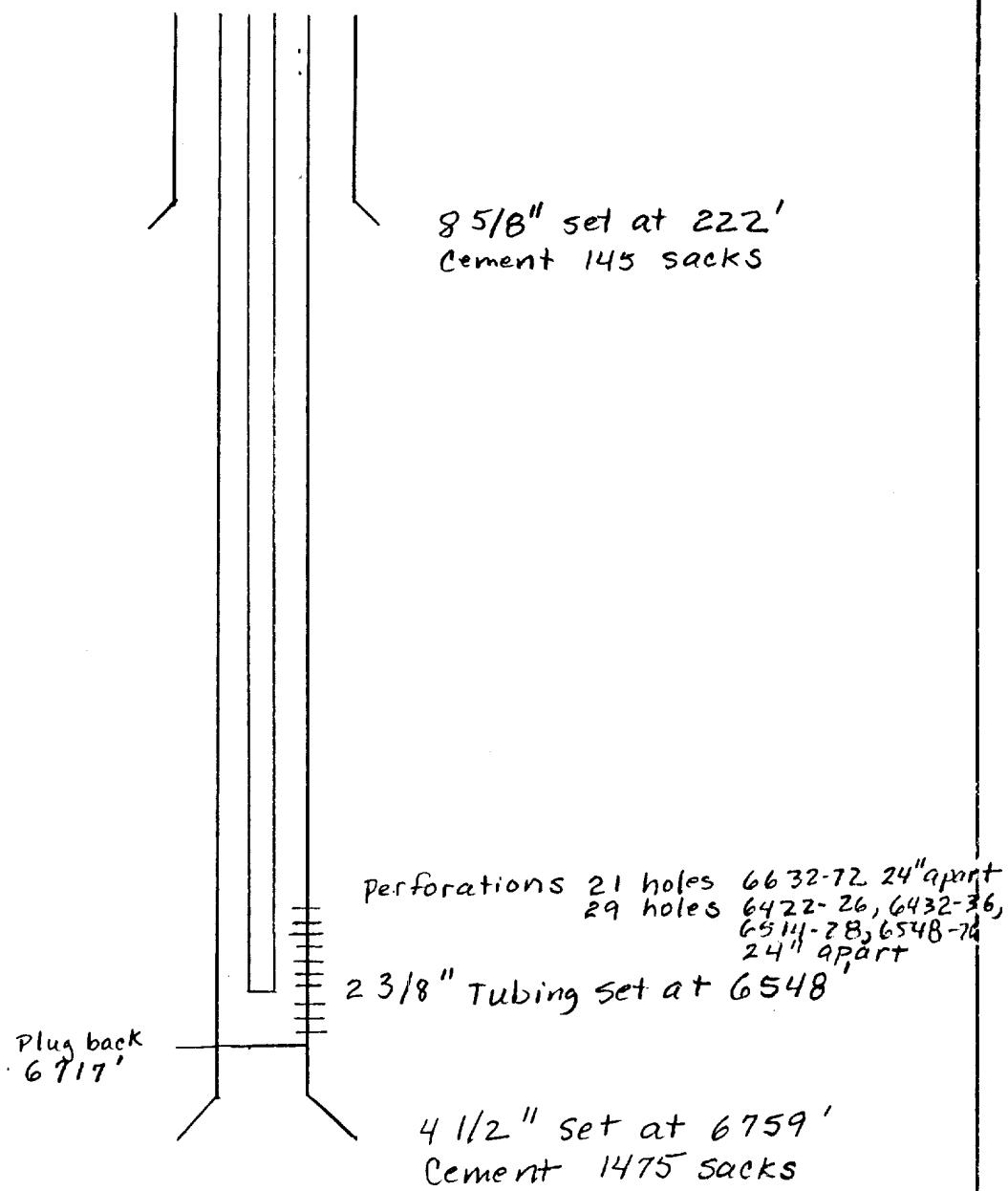


GEARHARTINDUCTION
ELECTRICAL LOG

FILING NO.					
	COMPANY <u>CURTIS J. LITTLE</u>				
	WELL <u>SALAZAR NO.4-R</u>				
	FIELD <u>BASIN DAKOTA</u>				
	COUNTY <u>RIO ARRIBA</u> STATE <u>NEW MEXICO</u>				
	LOCATION: <u>1630'FNL x 1460'FWL</u>				Other Services <u>CDL/CNL/GR</u>
	SEC <u>34</u>	TWP <u>25N</u>	RGE <u>6W</u>		
Permanent Datum	<u>GROUND LEVEL</u>			Elev. <u>6378</u>	Elevations:
Log Measured from	<u>K.B.</u>			<u>13</u> Ft. Above Permanent Datum	KB <u>6391</u>
Drilling Measured from	<u>K.B.</u>			DF <u>6390</u>	GL <u>6378</u>
Date	<u>1-27-84</u>				
Run No.	<u>ONE</u>				
Depth-Driller	<u>6753</u>				
Depth-Logger	<u>6753</u>				
Bottom Logged Interval	<u>6752</u>				
Top Logged Interval	<u>211</u>				
Casing-Driller	<u>8 5/8</u>	@ <u>222</u>	@	@	@
Casing-Logger	<u>21.1</u>				
Bit Size	<u>7 7/8</u>				
Type Fluid in Hole	<u>GEL</u>				
Density and Viscosity	<u>9.0</u>	<u>60</u>			
pH and Fluid Loss	<u>7.5</u>	<u>7</u> cc	cc	cc	cc
Source of Sample	<u>Mud Pit</u>				
Rm @ Meas. Temp.	<u>1.8</u> @ <u>74</u> °F		@ °F	@ °F	@ °F
Rmf @ Meas. Temp.	<u>1.4</u> @ <u>69</u> °F		@ °F	@ °F	@ °F
Rmc @ Meas. Temp.	<u>1.2</u> @ <u>68</u> °F		@ °F	@ °F	@ °F
Source at Rmf and Rmc	<u>M</u>	<u>M</u>			
Rm @ BHT	<u>----</u> @ <u>180</u> °F		@ °F	@ °F	@ °F
Time					
End Circulation	<u>20:00</u>				
Logger on Bottom	<u>02:47</u>				
Max. Rec. Temp. Deg. F.	<u>180</u> °F				
Equip. No. and Location	<u>7607</u>	<u>29-062</u>			
Recorded By	<u>Mease</u>				
Witnessed By	<u>Mr. Curtis Little</u>				



Kimbell Oil of TX [well-drawn sketch]

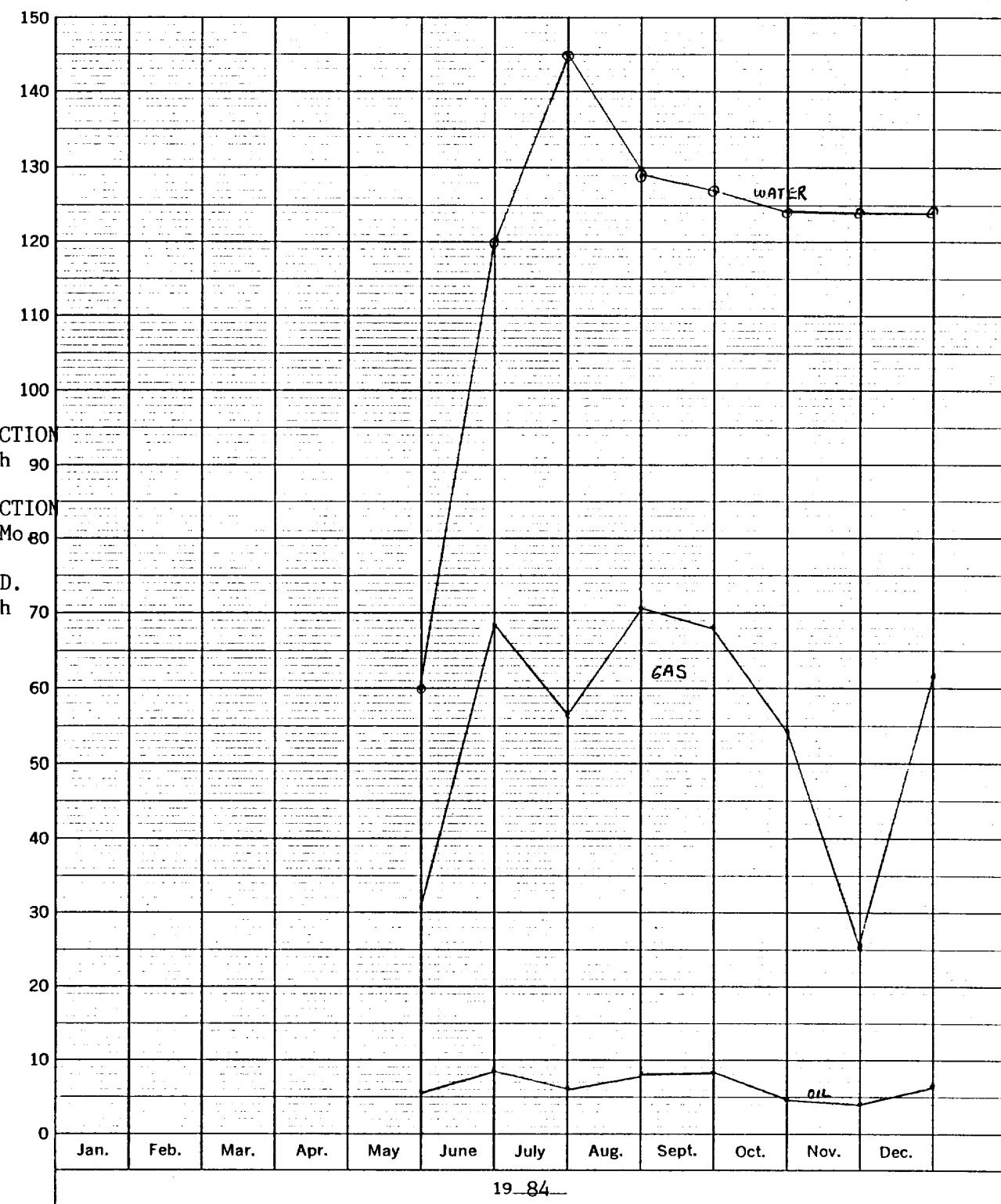


PRODUCTION TABLE

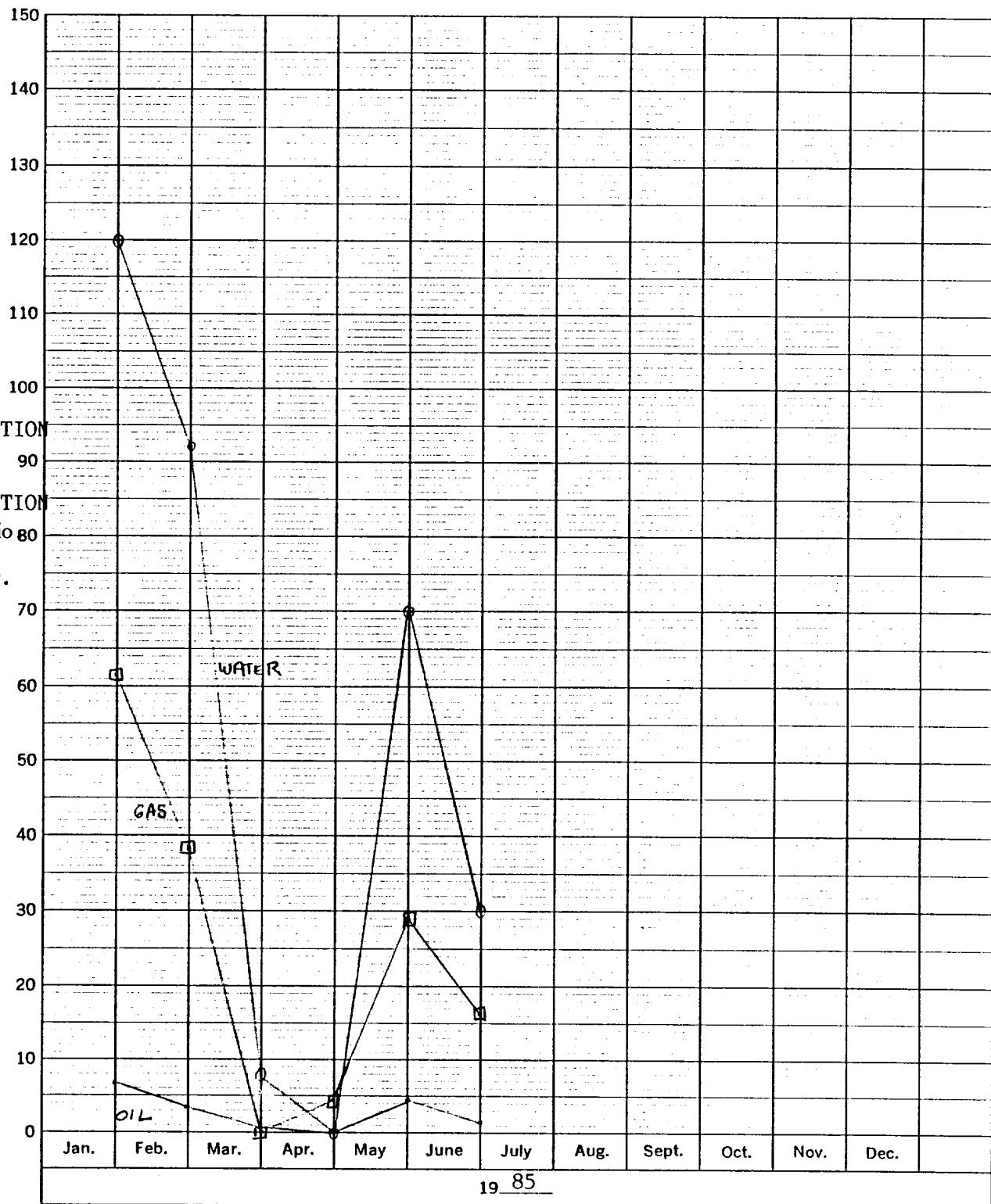
WELL NAME Salazar Federal 4-E
WELL LOCATION F-34-25N-6W
Perfs 6422-6672

Completion Date 2-21-84
Initial Potential 4984 MCF/day
Initial Pressure CP= 787
Initial GOR/Gravity -----

Basin Dakota
 Kimbell Oil Co. of TX
 Salazar Federal Well No. 4-E
 F-34-25N-6W
 Rio Arriba, New Mexico
 Date Production began: May 1984



Salazar Federal Well No. 4-E
Continued



NEW MEXICO OIL CONSERVATION COMMISSION
WELL DELIVERABILITY TEST REPORT FOR 19 84

Form C122-A
Revised 1-1-66

POOL NAME Basin Dakota	POOL SLOPE n = .75	FORMATION Dakota	COUNTY Rio Arriba
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COMPANY Bing Oil Company, Inc.			WELL NAME AND NUMBER Salazar 4E		
UNIT LETTER F	SECTION 34	TOWNSHIP 25N	RANGE 6W	PURCHASING PIPELINE El Paso Natural Gas Co.	
CASING O.D. - INCHES 4.500	CASING I.D. - INCHES 4.000	SET AT DEPTH - FEET 6759	TUBING O.D. - INCHES 2.375	TUBING I.D. - INCHES 1.995	TOP - TUBING PERF. - FEET 61,22
FROM 6122	TO 6672	CASING	WELL PRODUCING THRU X	GAS GRAVITY .661	GRAVITY X LENGTH 4245
FROM 7-12-84	TO 7-20-84	DATE OF FLOW TEST		DATE SHUT-IN PRESSURE MEASURED 7-27-84	

PRESSURE DATA - ALL PRESSURES IN PSIA

(a) Flowing Casing Pressure (DWt)	(b) Flowing Tubing Pressure (DWt)	(c) Flowing Meter Pressure (DWt)	(d) Flow Chart Static Reading	(e) Meter Error (Item c - Item d)	(f) Friction Loss (a - c) or (b - c)	(g) Average Meter Pressure (Integr.)
812	637	322	317	+5	315	311
(h) Corrected Meter Pressure (g + e)	(i) Avg. Wellhead Press. $P_t = (h + f)$	(j) Shut-In Casing Pressure (DWt)	(k) Shut-In Tubing Pressure (DWt)	(l) $P_c = \text{higher value of (j) or (k)}$	(m) Del. Pressure $P_d = \frac{50}{669} \% P_c$	(n) Separator or Dehydrator Pr. (DWt) for critical flow only 635
316	637	1337	1337	1337	669	

FLOW RATE CORRECTION (METER ERROR)

Integrated Volume - MCF/D 2295	Quotient of $\frac{\text{Item c}}{\text{Item d}}$ 1.0158	$\sqrt{\frac{\text{Item c}}{\text{Item d}}}$ 1.0079	Corrected Volume 2313 MCF/D
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WORKING PRESSURE CALCULATION

$(1 - e^{-\beta})$.266	$(P_c Q_m)^2 (1000)$ 472,923	$R^2 =$ $(1 - e^{-\beta}) (P_c Q_m)^2 (1000)$ 125,798	P_t^2 405,769	$P_w^2 = P_t^2 + R^2$ 531,567	$P_w = \sqrt{P_w^2}$ 729
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DELIVERABILITY CALCULATION

$D = Q \left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n =$ 2313	$\left[\left(\frac{1,340,008}{1,256,128} \right)^n \left(\frac{1.0667}{1} \right)^n = \frac{1,0496}{1} \right] =$ 2428	MCF/D
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REMARKS:

This well has critical flow -
Use FTP (b) for P_t (i).

SUMMARY

Item h	316	Psi
P _c	1337	Psi
Q	2313	MCF/D
P _w	729	Psi
P _d	669	Psi
D	2428	MCF/D

Company	SIMS OIL COMPANY, INC.
By	E. A. Clement
Title	Prod. Supt.
Witnessed By	
Company	

NEW MEXICO OIL CONSERVATION COMMISSION
WELL DELIVERABILITY TEST REPORT FOR 19 85

Form C122-A
 Revised 1-1-66

POOL NAME Basin Dakota	POOL SLOPE n = .75	FORMATION Dakota	COUNTY Rio Arriba
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Meter No. 94-932

COMPANY Kimbell Oil Company of Texas			WELL NAME AND NUMBER Salazar No. 48		
UNIT LETTER F	SECTION 34	TOWNSHIP 25N	RANGE 6W	PURCHASING PIPELINE El Paso Natural Gas Co.	
CASING O.D. - INCHES 4.500	CASING I.D. - INCHES 4.000	SET AT DEPTH - FEET 6759	TUBING O.D. - INCHES 2.375	TUBING I.D. - INCHES 1.995	TOP - TUBING PERF. - FEET 6422
FROM 6422	TO 6672	CASING	TUBING X	GAS GRAVITY .704	GRAVITY X LENGTH 4521
FROM 5/27/85	TO 6/1/85	DATE OF FLOW TEST	WELL PRODUCING THRU	DATE SHUT-IN PRESSURE MEASURED 6/18/85	

PRESSURE DATA - ALL PRESSURES IN PSIA

(a) Flowing Casing Pressure (DWt)	(b) Flowing Tubing Pressure (DWt)	(c) Flowing Meter Pressure (DWt)	(d) Flow Chart Static Reading	(e) Meter Error (Item c - Item d)	(f) Friction Loss (a - c) or (b - c)	(g) Average Meter Pressure (Integr.)
932	787	262	256	.06	525	259
(h) Corrected Meter Pressure (g + e)	(i) Avg. Wellhead Press. $P_t = (h + f)$	(j) Shut-In Casing Pressure (DWt)	(k) Shut-In Tubing Pressure (DWt)	(l) $P_c = \text{higher value of (j) or (k)}$	(m) Del. Pressure $P_d = \frac{40}{529} \% P_c$	(n) Separator or Dehydrator Pr. (DWt) for critical flow only 784
265	787	1322	1322	1322	529	

FLOW RATE CORRECTION (METER ERROR)

Integrated Volume - MCF/D	Quotient of $\frac{\text{Item c}}{\text{Item d}}$	$\sqrt{\frac{\text{Item c}}{\text{Item d}}}$	Corrected Volume
2035	1.0234	1.0116	2059 MCF/D

WORKING PRESSURE CALCULATION

$(1 - e^{-R})$	$(F_e Q_m)^2 (1000)$	$R^2 = (1 - e^{-R}) (F_e Q_m)^2 (1000)$	P_t^2	$P_w^2 = P_t^2 + R^2$	$P_w = \sqrt{P_w^2}$
.280	374,759	104,933	619,369	724,302	851

DELIVERABILITY CALCULATION

$D = Q \left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n = 2059 \left[\left(\frac{1,467,843}{1,023,483} \right)^n \right] = \frac{1,4341}{1,3105} = 1.098$	MCF/D
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REMARKS:

This well has critical flow -
 Use FIP (b) for P_t (1)

SUMMARY

Item h	265	Psi
P _c	1322	Psi
Q	2059	MCF/D
P _w	851	Psi
P _d	529	Psi
D	2692	MCF/D

Company **Kimbell Oil Company of Texas**
 By **E. A. Clement**
 Title **Prod. Supt.**

Witnessed By _____
 Company _____

$$G = 43560 (\phi)(1-S_w) \frac{(BHP_z)}{TR} (35.3) (A) (h)$$

G = original gas in place, cf

ϕ = porosity

S_w = water saturation

BHP_z = initial Bottom hole Pressure / \pm , psi

TR = temperature Reservoir, $^{\circ}$ R

A = Area of drainage, acres

h = thickness, feet

Given:

BHP_z est = 1900 psi

TR = 640° R

h = 90 ft

Assume:

ϕ = 10% (field avg)

S_w = 40% (" ")

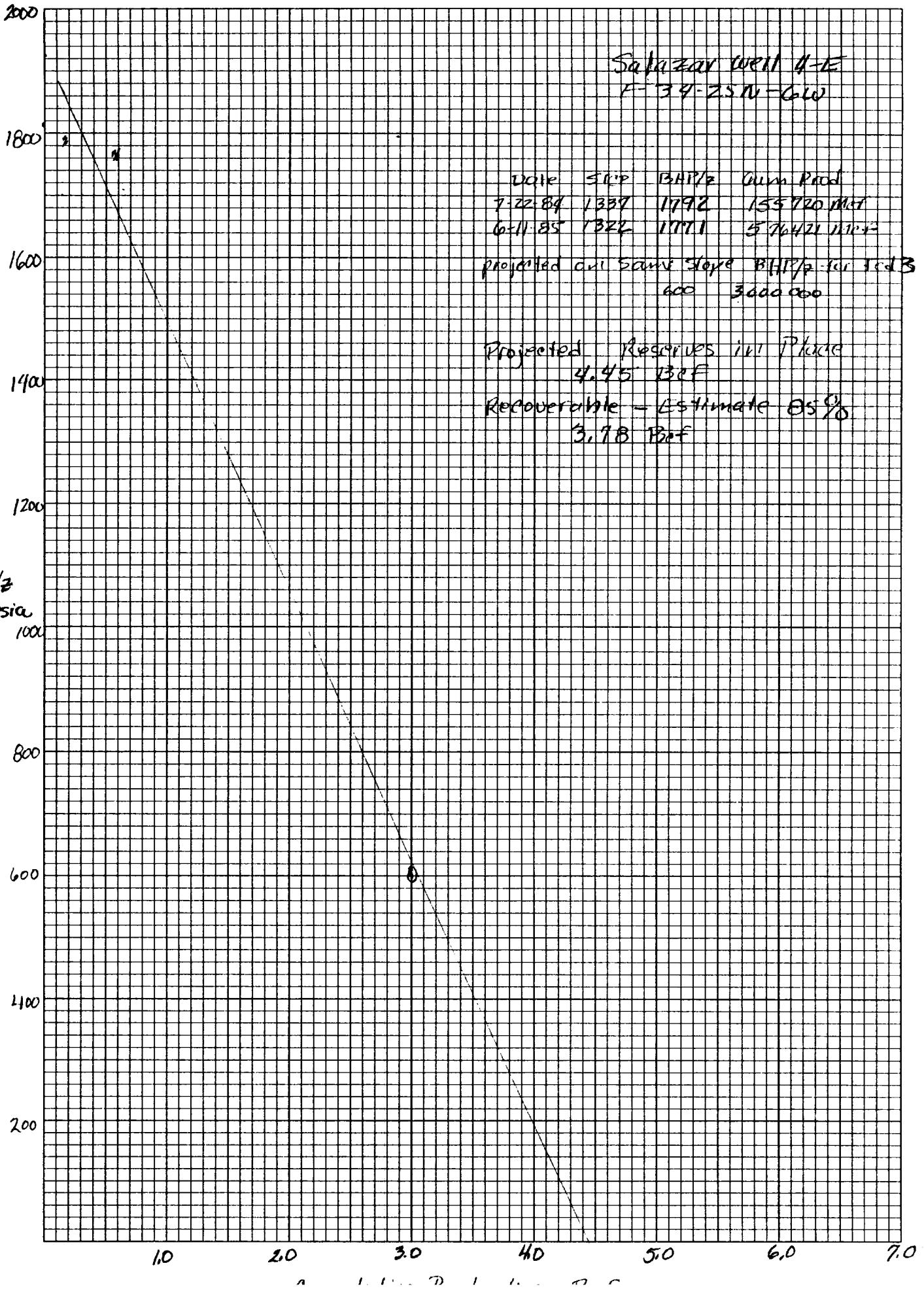
A = 160 acres

Solution:

$$G = 43560 (.10) (1-.40) \frac{1900}{640} (35.3) (160) (90)$$

$$= 3,944,188,420 \text{ cf}$$

$$\text{or } 3.95 \text{ Bcf}$$



PRODUCTION TABLE

WELL NAME Farming E No. 3-E

Completion Date 1981

WELL LOCATION D-2-24N-6W

Initial Potential

Perfs

Initial Pressure

Initial GOR/Gravity

PRODUCTION TABLE

WELL NAME Salazar Well No. 4

Completion Date

WELL LOCATION H-34-25N-6W

Initial Potential

Perfs

Initial Pressure

Initial GOR/Gravity

PRODUCTION TABLE

WELL NAME Federal Well No. 3
WELL LOCATION L-34-25N-6W
Perfs 6518-6662

Completion Date 11-1-63
Initial Potential 6152 MCF/Day
Initial Pressure SICP = 2322
Initial GOR/Gravity

PRODUCTION TABLE

WELL NAME Federal Well No. 3-E
WELL LOCATION I-34-2N-6W
Perfs 6509-6720

Completion Date 6-9-80
Initial Potential 2227 MCF/Day
Initial Pressure CP= 385
Initial GOR/Gravity

LIST OF ADJACENT WELLS/OPERATORS

Operator	Well Name	Well Location	Proration Unit
Merrion (abd)	Sal. G. Com 26 1	m-26-25N-6W	W $\frac{1}{2}$ section 26
Kimbell	Sal. Fed. 3	h-27-25N-6W	E $\frac{1}{2}$ section 27
Kimbell	Coral 2	m-27-25N-6W	W $\frac{1}{2}$ section 27
Merrion	Old Rock Com 2	p-28-25N-6W	E $\frac{1}{2}$ section 28
El Paso	Can. Largo Ut 135	h-33-25N-6W	E $\frac{1}{2}$ section 33
Kimbell	Federal 3	l-34-25N-6W	S $\frac{1}{2}$ section 34
	Federal 3-E	i-34-25N-6W	
Kimbell	Federal A 3	m-35-25N-6W	W $\frac{1}{2}$ section 25
	Federal A 3-E	e-35-25N-6W	

Sailor well 4-E

1630N 1460W Section 34

Township 25 N, Range 6 W

Meridian:

Dakota Wells