

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-10-84	
Company Consolidated Oil & Gas				Connection Gas Company of New Mexico			
Pool Basin Dakota				Formation Dakota			
Completion Date 11-12-84		Total Depth 8480		Plug Back TD 8424		Elevation 7239' GR	
Csg. Size 5 1/2		Wt. 15.5		Set At 8469		Perforations: From 8190 To 8388	
Tub. Size 1 1/2		Wt. 2.9		Set At 8321		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual gas						Packer Set At 7850	
Producing Thru Tbg		Reservoir Temp. °F #		Mean Annual Temp. °F		Baro. Press. - P _a	
L		H		G _g .650		% CO ₂ % N ₂ % H ₂ S	
						Prover 6" pos.	
						Meter Run choke nipple	
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	x	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.
1.	14 days						1520
2.	2" x 3/4" pos. choke						74
3.							60
4.							
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	11.00		86	1.000	1.240	1.000	1173
2.							
3.							
4.							
5.							
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.		
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.		
2.					Specific Gravity Separator Gas _____ X X X X X X X X		
3.					Specific Gravity Flowing Fluid _____ X X X X X		
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.		
5.					Critical Temperature _____ R _____ R		
P _c 1532 P _c ² 2347024							
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0135$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0100$		
1.			31299	2315725			
2.							
3.							
4.							
5.					AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1185$		
Absolute Open Flow 1185					Mcf @ 15.025		Angle of Slope @ 53.13°
Slope, n 0.75							
Remarks:							
Approved By Division		Conducted By:		Calculated By:		Checked By:	

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