

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

OIL CON. COM.

Type Test ☐ Initial ☐ Annual ☒ Special						Test Date 7-20-76					
Company Union Oil Company of Calif.						Connection None					
Pool Basin Dakota						Formation Dakota					
Completion Date 7-18-76			Total Depth 6225'			Plug Back TD 6180'		Elevation 6541' GL		Farm or Lease Name Navajo L-18	
Csg. Size 5-1/2"	Wt. 15 1/2 & 17	d -	Set At 6226'	Perforations: From 6063' To 6133'				Well No. 8			
Tbg. Size 2-3/8"	Wt. 4.7	d 1.995	Set At 5820'	Perforations: From None To				Unit L	Sec. 18	Twp. 25N	Rge. 10W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 5813'		County San Juan			
Producing Thru Tubing		Reservoir Temp. °F 157° @ 6219'		Mean Annual Temp. °F 50°		Baro. Press. - P _a 12.2		State New Mexico			
L 5813'	H 5813'	G _g 0.726 (est)	% CO ₂ 0.49%	% N ₂ 1.58%	% H ₂ S 0	Prover	Meter Run 3"	Taps Flange			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	7 Days						2020	-	PKR	-	S.I.
1.	3.0"		1-3/4"	200	43	60	1960	-	"	-	6 Hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	15.61	95.52	212.2	1.00	1.174	1.027	1800
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ None _____ Mcf/bbl.		
1.	0.317	520	1.30	.948	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.		
2.					Specific Gravity Separator Gas 0.726		
3.					Specific Gravity Flowing Fluid _____		
4.					Critical Pressure _____ P.S.I.A.		
5.					Critical Temperature _____ R		

P _c 2032.2	P _c ² 4129.8		
NO.	P _t ²	P _w	P _w ²
1	3,889.6	1987	3948.2
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 22.74$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 10.41$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 18,738$$

Absolute Open Flow	18,738	Mcf/d @ 15.025	Angle of Slope θ	Slope, n 0.75
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Remarks: Flow rate tested during flow clean up following the frac job and prior to shut in for 7 day build up - Information only.

Approved By Commission:	Conducted By: B. L. Griffith	Calculated By: J. D. Roe	Checked By: J. D. Roe <i>for</i>
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