## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS Revised 12-1-55

	Undesign	ated	<del></del>	Form	rrion_	FACU	red off	119	_county_	MJO A	rriba
niti	ialX_		Annual_		-	Spec	ial		_Date of	Test_	7-1-57
mpa	any Magnol	lia Petr	oleum C	ompany	L	ease	Jicaril	re alle	Wel	1 No	3 PC
it	M S	ec <b>15</b>	_Two	27N	Rge	. 3W	Purc	haser	Pacific No	rthwee	t
sin	ng <b>7-5/8</b> W	t. 2h#	I.D.	7.025	Set	at <b>423</b>	<b>5</b> Pe	rf	)1	То	38921
bin	ng <b>2-3/8"</b> W	t. 4.71	I.D.	1.995*	Set	at_ <b>384</b>	<b>51</b> Pe	erf		То	•
s F	Pay: From_	38601	To_ <u>3892</u>	, I	381	5' x	G			Bar.Pr	ess. <b>12 peia</b> (
odu	cing Thru:	Casi	ng		Tub	ing	x	Type We	11 6.0	. Dual	
							Sin	gle-Brade	nhead-G.	G. or	G.O. Dual
		<del></del>			•		ED DATA	<del></del>			· · · · · · · · · · · · · · · · · · ·
ste	d Through	(80000	(Chok	re) (100	peepk				Type Tap	s	
	( <del>5</del>		ow Data					Data	Casing D		<del></del>
	(Line)	(Ociob	00t)		1			Temp.			Duration of Flow
-	Size	Size	e ps	sig	h <sub>w</sub>	o <sub>F</sub> .	psig <b>1069</b>	°F.		°F.	Hr.
T	2"	0.750	2	2.5	-	63	22.5		1069		3 Hours
$\vdash$											
	Coefficient (24-Hour) 12.3650		$\sqrt{h_{\mathbf{w}}p_{\mathbf{f}}}$		а.	Ft		Factor F <sub>g</sub>	Factor F <sub>pv</sub>		@ 15.025 psia
├	12 × 3030			34.0	<b>-</b>	-9971		.9393	-		399.5
							1				
	quid Hydrod y of Liquid 9.402			-		SSURE CA	ALCUIATI	Speci Speci	fic Gravi fic Gravi <b>1081</b>	ty Flor	arator Gas wing Fluid <b>0.6</b> <b>1168.6</b>
rit	quid Hydrod		carbons	5)		ef/bbl. deg.		Speci Speci	fic Gravi	ty Flor	wing Fluid 0.66 1168.6
ity	quid Hydrod y of Liquid 9.402	l Hydrod	carbons(1-e	5)		ef/bbl. deg.	ALCUIATI	Speci Speci <sup>P</sup> c	fic Gravi 1081	ty Flor	wing Fluid <u>0.66</u> 1168.6
rit;	quid Hydrod y of Liquid 9.402 P <sub>w</sub>	l Hydrod	carbons(1-e	5)		ef/bbl. deg.		Speci Speci Pc P <sub>w</sub> 2	fic Gravi <b>1081</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	ty Flor	wing Fluid 0.66 1168.6
it	quid Hydrod y of Liquid 9.402 P <sub>w</sub>	l Hydrod	carbons(1-e	5)		ef/bbl. deg.		Speci Speci Pc P <sub>w</sub> 2	fic Gravi <b>1081</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	ty Flor	wing Fluid 0.66 1168.6
olu	quid Hydrod y of Liquid 9.402 Pw (psia) 212	Pt	F <sub>c</sub> Q	s) (F	<sub>e</sub> Q) <sup>2</sup>	ef/bbl.deg.		Speci Speci Pc P <sub>w</sub> 2	fic Gravi <b>1081</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	ty Flor	wing Fluid 0.66 1168.6
olu PAN	quid Hydrod y of Liquid 9.402  Pw (psia) 212  ute Potenti NY Magne SSP.O. Box 2	Pt lial:	F <sub>c</sub> Q	S) (F	Q) <sup>2</sup>	CFPD;	n_ <b>c.</b>	Speci Speci Pc P <sub>w</sub> 2	fic Gravi <b>1081</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	ty Flor	wing Fluid 0.66 1168.6
vity solu MPAN DRES	quid Hydrod y of Liquid 9.402  Pw (psia) 212  ute Potenti	Pt lial:	F <sub>c</sub> Q	S) (F	Q) <sup>2</sup>	CFPD;	Q) <sup>2</sup> -e-s)	Speci Speci Pc P <sub>w</sub> 2	fic Gravi 1081 P <sub>c</sub> -P <sub>w</sub> <sup>2</sup> 1123.7	ty Flor	wing Fluid 0.6  1168.6  Pw Pc

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 60° F.
- $P_c$ = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- $P_{w}$  Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- P<sub>f</sub> Meter pressure, psia.
- $h_{\mathbf{w}}$ Differential meter pressure, inches water.
- Fg Gravity correction factor.
- $F_t$  Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If Pw cannot be taken because of manner of completion or condition of well, then Pw must be calculated by adding the pressure drop due to friction within the flow string to PtOIL CONSERVATION COMMISSION

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