## Revised 12-1-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

	Pasin I	akota	F	Formation Daketa				County_ Ric Arriba			
Ini	itial X	A1	nnual	Special				Date of	Test	11-9-62	
Con	ompany Carlbins Cil Company			Lease Bree			Well No. D-1				
Uni	.t <b>D</b>	Sec	Twp . 27 1	Rg_Rg	e. 6 W	Purc	haser	louthern U	nion Gar	Company	
	ing A										
Tub	oing 2-3/8"	Wt. 4.7	_I.D. <u>1.</u>	<b>)}</b> 5 _Se	t at 73	<b>3</b> Fe	erf	7343	То		
	Pay: From			••	,	•					
	ducing Thru					ls	Type W	ell <b>Min</b> e	le Gas		
	e of Complet					Sin	gle-Brad	enhead-G.	G. or G	.O. Dual	
	-					ED DATA		<del>-</del>			
Тес	ted Through	(Prover)	(Choke)	(Moton)		OD DAIA		M a Ma	_		
			Data	(Meter)		m ) ;		Type Tap			
	(Prover)	(Choke)	Press	Diff.	Temp.	Tubing Press.		Casing D	ata Temp.		
No.	(Line) Size	(Orifice Size		h <sub>w</sub>	o <sub>F</sub> .	psig	°F.	psig	∍ <sub>F</sub> .	of Flow Hr.	
SI l.		2/12				2350		2360			
2.		3/4"				340		1190			
3. 4.							<u> </u>				
5.							I				
<u>_</u>	Coeffici	ent		essure	Flow CALC		S Gravity	I Communi		ate of Flow	
No.	(24-Hour) $\sqrt{h_{WP}}$			_		or	Factor	Factor		Q-MCFPD @ 15.025 psia	
1.	14.1405			372			.9535	1.04		5254	
3.											
				PRE	ESSURE CA	LCUTATE	ons				
	Liquid Hydro ity of Liqui							fic Gravit			
	רוומנה.ו זה עדו	~ HTTM TO A 4 4	rbons		deg.		Cmaai		.v Flowi	ng Fluid	
		-	(1-e <sup>-s</sup> )				pc	.fic Gravit	P <sub>C</sub>		
`—	•	-					pc	.iic Gravit	P2		
-1	•		_(1-e <sup>-s</sup> )_	(F <sub>2</sub> Q) <sup>2</sup>		0)2	Pc	<u> </u>	Pc		
lo .		-		$(F_cQ)^2$	(F <sub>C</sub>	Q) <sup>2</sup> e <sup>-s</sup> )	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	P <sub>C</sub> Cal	P <sub>W</sub> P <sub>C</sub>	
lo .	P <sub>w</sub>		_(1-e <sup>-s</sup> )_	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>C</sub>	Q) <sup>2</sup> e-s)	Pc	<u> </u>	PC	. P	
No.	P <sub>w</sub>		_(1-e <sup>-s</sup> )_	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>C</sub>	Q) <sup>2</sup> e-s)	P <sub>c</sub>	<u> </u>	PC	P <sub>W</sub> P <sub>C</sub>	
	P <sub>w</sub> Pt (psia)	Pt Pt	(1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	(Fc (1-	e-s)	P <sub>c</sub>	<u> </u>	PC	P <sub>W</sub> P <sub>C</sub>	
lo.	Pw Pt (psia) Plute Potent	Pt	(1-e <sup>-s</sup> )		(Fc (1-	Q) <sup>2</sup> e-s) n_1,21	P <sub>c</sub>	<u> </u>	PC	P <sub>W</sub> P <sub>C</sub>	
bso OMP GEN	Pw Pt (psia) Plute Potent PANY ESS	Pt ial:	(1-e <sup>-s</sup> )	w Navie	(Fc (1-	n_1,21,	P <sub>c</sub>	<u> </u>	PC	P <sub>W</sub> P <sub>C</sub>	
No.	Pw Pt (psia) Pute Potent	Pt ial:	(1-e <sup>-s</sup> )	w Navie	(Fc (1-	n 1,24,	P <sub>c</sub>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal Pw	P <sub>W</sub> P <sub>C</sub> .503	
No.	Pw Pt (psia) Plute Potent PANY Control TESS Box	Pt ial:	(1-e <sup>-s</sup> )	w Navie	(Fc (1-	n 1,24,	P <sub>c</sub>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	PC	P <sub>W</sub> P <sub>C</sub>	

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## **NOMENCLATURE**

- Q I Actual rate of flow at end of flow period at W. H. working pressure  $(P_w)$ . MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub>= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
  psia
- Pw- Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_{\mathbf{w}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{w}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .