

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
FEB 02 1984
OIL CON. DIV.
DIST. 3

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 1/30/84							
Company Union Texas Petroleum Corp.			Connection El Paso Natural Gas Company								
Pool Basin			Formation Dakota		Unit						
Completion Date 1/2/84		Total Depth 6823		Plug Back TD 6790	Elevation 6362						
Csq. Size 7.000	Wt. 26.00 23.00	d 6.276 6.366	Set At 6823	Perforations: From 6564 To 6728							
Thq. Size 2.375	Wt. 4.70	d 1.995	Set At 6636	Perforations: From Open Ended To							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual - Gas - Oil				Packer Set At 6440							
Producing Thru Tubing		Reservoir Temp. *F	Mean Annual Temp. *F	Baro. Press. - P _a 12							
L 6626	H	G _g 0.700	% CO ₂	% N ₂	% H ₂ S						
Prover		Meter Run	Taps								
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	Duration of Flow
SI	2"		3/4"				1202				7 days
1.							120	68°			3 hours
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	12.3650		132	0.9924	0.9258	1.015	1522				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. *R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
P_c 1214 P_c^2 1,473,796 (1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0544$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0405$											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1584$						
1			75,989	1,397,807							
2											
3											
4											
5											
Absolute Open Flow 1584				Mcf/d @ 15.025				Angle of Slope ϕ		Slope, n 0.75	
Remarks:											
Approved By Division			Conducted By: Bruce Voiles			Calculated By: Ken Roddy			Checked By:		