

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 5/31/78			
Company Amoco Production Company				Connection					
Pool Choza Mesa				Formation Pictured Cliffs				Unit	
Completion Date 5-24-78		Total Depth 4325		Plug Back TD 4278		Elevation 7190		Farm or Lease Name Valencia Canyon Unit	
Csg. Size 4.500	Wt. 10.5	d 4.052	Set At 4325	Perforations: From 3951 To 4210		Well No. 23			
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 4159	Perforations: From Open To Ended		Unit Sec. Twp. Rge. B 15-23 28 4			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None		County Rio Arriba			
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L	H	Gg .65	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	7 days						1047		1040		
1.	2.375	0.750					100	60	570		3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		112	1.000	.9608	1.010	1344
2.							
3.							
4.							
5.							

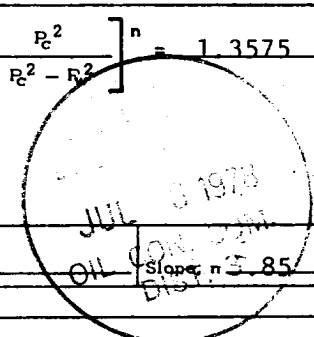
NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2.					Specific Gravity Separator Gas _____ X X X X X X X X	
3.					Specific Gravity Flowing Fluid _____ X X X X X	
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.	
5.					Critical Temperature _____ R _____ R	

P _c 1059 P _c ² 1121481				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		582	338724	782757
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.4327$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1824$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.3575$



Absolute Open Flow 1824 Mcfd @ 15.025		Angle of Slope θ
Remarks:		
Approved By Commission:	Conducted By:	Calculated By: T. M. Oliver