

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 6/30/78																																																																																																	
Company Amoco Production Company				Connection El Paso Natural Gas Company																																																																																																			
Pool Choza Mesa				Formation Pictured Cliffs				Unit																																																																																															
Completion Date 6/23/78		Total Depth 4500		Plug Back TD 4340		Elevation 7281		Farm or Lease Name Valencia Canyon Unit																																																																																															
Csq. Size 4.500	Wt. 10.5	d 4.052	Set At 4605	Perforations: From 4118 To 4300		Well No. 25																																																																																																	
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 4285	Perforations: From Open To Ended		Unit Sec. Twp. Rge. N 15 28 4																																																																																																	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At None		County Rio Arriba																																																																																															
Producing Thru		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico																																																																																															
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps																																																																																															
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="6">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td>7 days</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1028</td> <td></td> <td>1208</td> <td></td> <td></td> </tr> <tr> <td>1.</td> <td>2.375</td> <td></td> <td>0.750</td> <td></td> <td></td> <td></td> <td>350</td> <td>60</td> <td>725</td> <td></td> <td>3 hrs.</td> </tr> <tr><td>2.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>3.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>4.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>5.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> </table>										FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI	7 days						1028		1208			1.	2.375		0.750				350	60	725		3 hrs.	2.												3.												4.												5.											
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NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																																																																																																
1	12.365		362	1.000	0.9608	1.037	4460																																																																																																
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NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ X X X X X X X X Specific Gravity Flowing Fluid _____ X X X X X Critical Pressure _____ P.S.I.A. _____ P.S.I.A. Critical Temperature _____ R _____ R																																																																																																		
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P _c 1040 P _c ² 1081600 <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_t²</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> <tr> <td>1</td> <td></td> <td>737</td> <td>543169</td> <td>538431</td> </tr> <tr><td>2</td><td></td><td></td><td></td><td></td></tr> <tr><td>3</td><td></td><td></td><td></td><td></td></tr> <tr><td>4</td><td></td><td></td><td></td><td></td></tr> <tr><td>5</td><td></td><td></td><td></td><td></td></tr> </table>					NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	1		737	543169	538431	2					3					4					5					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.0088$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.8092$ AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 8069$																																																																				
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Absolute Open Flow 8069 Mcfd @ 15.025					Angle of Slope @		Slope, n .85																																																																																																
Remarks:																																																																																																							
Approved By Commission:			Conducted By: T. M. Oliver		Calculated By: TMO/KCW		Checked By: J. L. Krupka																																																																																																