

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8-1-78																																																																																																	
Company Jerome P. McHugh				Connection																																																																																																			
Pool Choza Mesa - PC				Formation Pictured Cliffs				Unit																																																																																															
Completion Date 7-14-78		Total Depth 4307'		Plug Back TD 4227'		Elevation 7213'		Farm or Lease Name Valencia Canyon																																																																																															
Csg. Size 4-1/2	Wt. 10.5#	d 4307'	Set At	Perforations: From 3986 To 4186		Well No. 38																																																																																																	
Tbg. Size 1-1/4	Wt. 2.4#	d 4119'	Set At	Perforations: From Open To End		Unit Sec. Twp. Rge. D 24 28 4																																																																																																	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County Rio Arriba																																																																																															
Producing Thru Tbg		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State NM																																																																																															
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps																																																																																															
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="6">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1100</td> <td></td> <td>1100</td> <td></td> <td>7 days</td> </tr> <tr> <td>1.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3.</td> <td>3/4 Pos. Choke</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>114</td> <td>70°</td> <td>660</td> <td></td> <td>3 hrs</td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>										FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI							1100		1100		7 days	1.												2.												3.	3/4 Pos. Choke						114	70°	660		3 hrs	4.												5.											
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NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																																																																																																
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3	12.365		126	.9905	.9837	1.009	1531																																																																																																
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NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ X X X X X X X X Specific Gravity Flowing Fluid _____ X X X X X Critical Pressure _____ P.S.I.A. _____ P.S.I.A. Critical Temperature _____ R _____ R																																																																																																		
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P _c 1112 P _c ² 1236544 <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_t²</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> <tr> <td>1</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>2</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3</td> <td></td> <td>672</td> <td>451584</td> <td>784960</td> </tr> <tr> <td>4</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>					NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	1					2					3		672	451584	784960	4					5					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.5753$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4714$ AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2253$																																																																				
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Absolute Open Flow 2253 Mcfd @ 15.025					Angle of Slope θ			Slope, n = .85																																																																																															
Remarks: Light spray of water at end of test																																																																																																							
Approved By Commission:			Conducted By: Hall			Calculated By: Hall			Checked By:																																																																																														