MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool	Blanco M	esaver	đe		Formation	Mesav	rerd e		County San Juan				
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ate	of Compte	tion:_	whire		Packe			neservo	orr remb•"				
							ED DATA						
Tested Through (Choke) (Meter)								Type Taps					
	(Prover)		Flow Da		s. Diff.	Temp.	Tubing	Data Temp.	Casing D	ata Temp.	1	Duration	
ю.	(Line)	(Ori	fice)			}		'		or.		of Flow	
_	Size	S	ize	psi.	g h _w	°F.	psig	°F.	psig	-F.	├	Hr.	
I		3/1	, M	126		65.5	1102	65.5				hours	
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io.	Coefficient (24-Hour)		$\sqrt{h_{W}}$		psia	Flow Temp. Factor Ft		Factor Fg	Factor F _{pv}		Q-M	Rate of Flow Q-MCFPD @ 15.025 psia	
	12.3650				138	0.9952		0.9463	1,01	•	1,	629	
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avit	iquid Hydr ty of Liqu 9,402	id Hyd	rocarb					Speci	fic Gravi fic Gravi 11 4	ty Sepa ty Flor PC 12	arato wing !41	r Gas Fluid	
•	P _w	Р	2 F	_c Q	(F _c Q) ²	· (1	(cQ) ² L-e-s)	P _w 2	$P_c^2 - P_w^2$		al. P _w	Pw Pc	
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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_w) . MCF/da. @ 15.025 psia and 60° F.
- P_c 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt- Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- P_{f} Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- F_t Flowing temperature correction factor.
- F_{DV} Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{L}}$.

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