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i Haran do	wthwest  Sec.  Wt. 15  Wt. 4  om 6036  ru: Ca  letion:  gh (Ch ) (Ori ) (Ori S  3  drocarbo  drocarbo  quid Hyd  ential:  uthwest 62 Petr.	Annument Productions Sec. 15 Two Wt. 15.5 If wt. 4.70 If om 6038 To ru: Casing letion: 12/8 If with the stee of th	Annual  withwest Production C  Sec. 15 Twp. 27N  Wt. 15.5 I.D. 4.  Wt. 4.70 I.D. 1.  om 6038 To 6056  ru: Casing letion: 12/8/60  Flow Data  r) (Choke) Press. (Orifice) Size psig  3/4" 448  drocarbon Ratio quid Hydrocarbons (1-e-s)  drocarbon Ratio quid Hydrocarbons (1-e-s)	### MULTI-POINT B.  #### Formation  Annual  ###################################	MULTI-POINT BACK PRES	### MULTI-POINT BACK PRESSURE TEST  #### Special	### MULTI-POINT BACK PRESSURE TEST FOR GASE  ###################################	######################################	MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS	

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## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ). MCF/da. @ 15.025 psia and 60° F.
- $P_c$ I 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw- Differential meter pressure, inches water.
- FgI Gravity correction factor.
- $F_t$  Flowing temperature correction factor.
- $F_{pv}$  Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .