Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

(Line) (1999333) psig h _w o _F . psig o _F .	12.0 Duratio of Flow
Southwest Production Company Lease Melloway Pederal Well No.	12.0 Duratio of Flow
Sing St Wt 15.5 I.D. 4.990 Set at 6595 Perf W 6348 To 6426	Duratio of Flowers
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Single-Brademeau-9.	Duratio of Flo Hr. day of Flow
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Type Taps	of Flow
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Time 3/4* 355 80 355 80 815 3-hr	of Flow
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FLOW CALCULATIONS Coefficient Pressure Flow Temp. Gravity Compress. Rate of Factor Factor Factor Factor Factor Factor Factor Factor Factor Fpv @ 15.02 12.3650	
Coefficient (24-Hour) $\sqrt{h_w p_f}$ Pressure Flow Temp. Gravity Compress. Rate of Factor Factor Factor F $_g$ F $_g$ F $_{pv}$ @ 15.02	
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PRESSURE CALCULATIONS	
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vity of Liquid Hydrocarbons deg. Specific Gravity Flowing Flue (1-e-5) Pc. 2042 Pc 4167.7	
P _c . 2042 P _c 4167.7 P _w 827 P _w 2 683.9	
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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure $(P_{\rm W})$. MCF/da. @ 15.025 psia and 60° F.
- P_C= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- F_g : Gravity correction factor.
- Ft Flowing temperature correction factor.
- F_{DV} Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\rm W}$ cannot be taken because of manner of completion or condition of well, then $P_{\rm W}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\rm t}$.

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