

Initial Deliverability  
TestNEW MEXICO OIL CONSERVATION COMMISSION  
GAS WELL TEST DATA SHEET - - SAN JUAN BASIN(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA  
EXCEPT BARKER DOME STORAGE AREA)

Pool Basin Dakota Formation Dakota County San Juan  
Purchasing Pipeline El Paso Natural Gas Company Date Test Filed January 8, 1962

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Operator Western Natural Gas Company Lease Schlosser-Federal Well No. 2  
Unit M Sec. 3 Twp. 27-N Rge. 11-W Pay Zone: From 6596 To 6626  
Casing: OD 5 1/2" WT. 15.5 Set At 6769 Tubing: OD 2 1/16 WT. 3.4 T. Perf. 6549  
Produced Through: Casing \_\_\_\_\_ Tubing X Gas Gravity: Measured .681 Estimated \_\_\_\_\_  
Date of Flow Test: From 11-26-61 To 12-4-61 \* Date S.I.P. Measured 12-11-61  
Meter Run Size 4.026 Orifice Size 2.250 Type Chart L-10 Type Taps Flange

## OBSERVED DATA

Flowing casing pressure (Dwt) Packer psig + 12 = \_\_\_\_\_ psia (c)  
Flowing tubing pressure (Dwt) 507 psig + 12 = 519 psia (b)  
Flowing meter pressure (Dwt) 459 psig + 12 = 471 psia (c)  
Flowing meter pressure (meter reading when Dwt. measurement taken:  
Normal chart reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (c)  
Square root chart reading (6.85)<sup>2</sup> x spring constant 10 = 469 psia (c)  
Meter error (c) - (d) or (d) - (c) ± \_\_\_\_\_ = + 2 psi (e)  
Friction loss, Flowing column to meter:  
(b) - (c) Flow through tubing: (a) - (c) Flow through casing = 48 psi (f)  
Seven day average static meter pressure (from meter chart):  
Normal chart average reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (c)  
Square root chart average reading (6.95)<sup>2</sup> x sp. const. 10 = 483 psia (c)  
Corrected seven day avge. meter press. (p<sub>f</sub>) (g) + (e) = 485 psia (f)  
P<sub>t</sub> = (h) + (f) = 533 psia (i)  
Wellhead casing shut-in pressure (Dwt) Packer psig + 12 = \_\_\_\_\_ psia (j)  
Wellhead tubing shut-in pressure (Dwt) 1475 psig + 12 = 1487 psia (k)  
P<sub>c</sub> = (j) or (k) whichever well flowed through = 1487 psia (l)  
Flowing Temp. (Meter Run) 89 °F + 460 = 549 °Abs (m)  
P<sub>d</sub> = ½ P<sub>c</sub> = ½ (l) = 744 psia (r)

## FLOW RATE CALCULATION

$$Q = \frac{1494}{(\text{integrated})} \times \left( \frac{\sqrt{(c)} = 21.70 = 1.002}{\sqrt{(d)} = 21.66} \right)^* = 1497 \text{ MCF/day}$$

## DELIVERABILITY CALCULATION

$$D = Q \frac{1497}{\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} = \frac{1,457,633}{1,813,008} \right]^n} = \frac{1497}{(0.9143)^{0.75}} = 1400 \text{ MCF/day}$$

## SUMMARY

P<sub>c</sub> = 1487 psia  
Q = 1497 Mcf/day  
P<sub>w</sub> = 631 psia  
P<sub>d</sub> = 744 psia  
D = 1400 Mcf/day

Company Western Natural Gas Company  
By SPR Gook  
Title Division Petroleum Engineer  
Witnessed by Paul Varner  
Company Western Natural Gas Company

- \* This is date of completion test.  
\* Meter error correction factor

## REMARKS OR FRICTION CALCULATIONS

GL	(1-e <sup>-S</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> R <sup>2</sup>	(1-e <sup>-S</sup> )	P <sub>t</sub> <sup>2</sup> (Column i)	P <sub>t</sub> <sup>2</sup> + R <sup>2</sup>	P <sub>w</sub>
4460	0.264	433.847	114.536		284.089	398.625	631

$$F_c = 13.914; \text{ tbg ID} = 1.75"$$

