

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 11-1-77	
Company Getty Oil Company				Connection Not Connected		
Pool Blanco				Formation Mesa Verde		
Completion Date 10-24-77		Total Depth 4490		Plug Back TD 4450		Elevation 6047
Perforations: From 4317 To 4402						Well No. 1"A"
Csg. Size 7.0-4.5		Wt. 20.0	d 6.456	Set At 2392	Unit I Sec. 14 Twp. 27n Rge. 9W	
Thq. Size 2.375		Wt. 4.7	d 1.995	Set At 4392	From Open To Ended	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas					Packer Set At	
Producing Thru tubing					Baro. Press. - P_a	
Reservoir Temp. $^{\circ}F$ 720					Mean Annual Temp. $^{\circ}F$	
County San Jaun					State New Mexico	
L 4392		H 4392	Gg 720	% CO ₂	% N ₂	% H ₂ S
Prover 2.000		Meter Run		Taps		

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. $^{\circ}F$	Press. p.s.i.g.	Temp. $^{\circ}F$	Press. p.s.i.g.	Temp. $^{\circ}F$	
SI							847		847		168 Hr.
1.	2.000	X	.750				217		471		1 "
2.	2.000	X	.750				195		424		1 "
3.	2.000	X	.750				155		405		1 "
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor F_t	Gravity Factor F_g	Super. Compress. Factor F_{py}	Rate of Flow Q, Mcfd
1	11.00		229	1.000	1.179	1.030	3059
2	11.00		207	1.000	1.179	1.028	2760
3	11.00		167	1.000	1.179	1.022	2213
4.							
5.							

NO.	P_r	Temp. $^{\circ}R$	T_r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2.					Specific Gravity Separator Gas _____ X X X X X X X X	
3.					Specific Gravity Flowing Fluid _____ X X X X X	
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.	
5.					Critical Temperature _____ R _____ R	

P_c 859 P_c^2 737881				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.3083}{1.3083 - 0.0001} = 1.0001$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.2232}{1.2232 - 0.0001} = 1.0001$	
NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2707$		
1							
2							
3	27889	417	173889	563992			
4							
5							

Absolute Open Flow 2,707 Mcfd @ 15.025		Angle of Slope ϕ _____		Slope, n .75	
Remarks: Top of liner hanger 2273					
Approved By Commission:		Conducted By: Berhost		Calculated By: Berhost	
				Checked By: <i>K.P. Hunsicker</i>	