

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

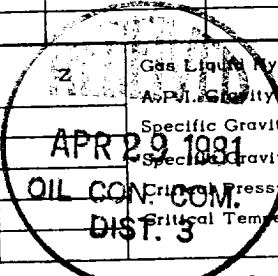
Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 4-13-81	
Company GETTY OIL COMPANY				Connection Not connected			
Pool Basin				Formation Dakota			
Completion Date 4-3-81		Total Depth 6104		Plug Back TD 6050		Elevation 5823 G.L.	
Csg. Size 5.500		Wt. 15.5		Set At 6104		Perforations: From 5967 To 6021	
Tbg. Size 2.375		Wt. 4.70		Set At 5972		Perforations: From OPEN To ENDED	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas						Packer Set At	
Producing Thru Tubing		Reservoir Temp. °F 6		Mean Annual Temp. °F		Baro. Press. - P _a 12.0	
L 5972		H 5972		G _g .700		% CO ₂ % N ₂ % H ₂ S	
Prover 2.000		Meter Run		Taps			

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1509		1509		192HRSI
1.	2.000 x .750						524	60	1181		1st hr.
2.	2.000 x .750						450	60	990		2nd hr.
3.	2.000 x .750						409	60	903		3rd hr.
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	11.000		536	1.000	1.195	1.069	7454
2	11.000		462	1.000	1.195	1.058	6425
3	11.000		421	1.000	1.195	1.052	5822
4.							
5.							

NO.	P _t	Temp. °R	T _r	Gas Liquid Hydrocarbon Ratio 1,000 to 1 BL Mcf/bbl.
1				As P.L. Gravity of Liquid Hydrocarbons 59.60 Deg.
2.				Specific Gravity Separator Gas X X X X X X X X
3.				Specific Gravity Flowing Fluid X X X X X
4.				Critical Pressure P.S.I.A. P.S.I.A.
5.				Critical Temperature R R



P _c 1521	P _c ² 2313441	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.5671$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4007$
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²		
1						
2						
3	177241	915	837225	1476216	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 8,155$	
4						
5						

Absolute Open Flow 8,155 Mcfd @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks:

Approved By Commission:	Conducted By: Paul D. Berhost	Calculated By: Paul D. Berhost	Checked By:
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