

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 6-15-84	
Company Beta Development Co.		Connection El Paso	
Pool Basin Dakota		Formation Dakota	
Completion Date 5-11-84		Total Depth 6540	Plug Back TD 6502
Elevation 6121		Farm or Lease Name Holloway Federal	
Csq. Size 4.5	Wt. 10.5	Set At 6540	Perforations: From 6290 To 6488
Thg. Size 1.25	Wt. 2.4	Set At 6462	Perforations: From open To ended
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single		Packer Set At None	County
Producing Thru Tubing	Reservoir Temp. °F #	Mean Annual Temp. °F	Baro. Press. - P _a
L	H	G _g 680	% CO ₂ % N ₂ % H ₂ S Prover Meter Run Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							1114		1127	
1.	2"		.750	133	97	65	192		798	
2.	2"		.750	108	79	63	174		712	1 hr
3.	2"		.750	92	67	62	166		680	1 hr
4										1 hr
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	12.3650		104	.9933	.9393	1.012	1214
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.					9 bbls oil	580				
2.					193,000 to 1 Mcf/bbl.					
3.										
4.										
5.										

P _c 1126	P _c ² 1267876	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.606916$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4272$
NO. 1	P _r ² 692	P _w ² 478864	P _c ² - P _w ² 789012
2.			
3.			
4.			
5.			

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1,733$$

Absolute Open Flow 1,733 Mcfd @ 15.025 Angle of Slope 0 Slope, n .75

Remarks:

Approved By Division Conducted By: John R. Keeling Calculated By: John R. Keeling Checked By: