

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 11/21/84		RECEIVED FEB 27 1985 OIL CON. DIV. DIST. 3											
Company Tenneco Oil Company				Connection													
Pool Basin				Formation Dakota													
Completion Date		Total Depth 6660		Plug Back TD 6649		Elevation		Farm or Lease Name Bolack B									
Csg. Size 7 4 1/2		Wt. d		Set At 3440 6657		Perforations: From 6486 To 6632		Well No. 8E									
Trg. Size 2 3/8		Wt. d		Set At 6547		Perforations: From To		Unit Sec. Twp. Rge. B 33 28 8									
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County San Juan									
Producing Thru		Reservoir Temp. °F p		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico									
L		H		Gg .700		% CO ₂		% N ₂		% H ₂ S		Prover		Meter Run		Taps	
FLOW DATA										TUBING DATA			CASING DATA			Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F							
SI							2125		2105								
1.	2 x 6 x .75						82		362	54					3 hours		
2.																	
3.																	
4.																	
5.																	
RATE OF FLOW CALCULATIONS																	
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd										
1	11		94	1.006	1.195	1.0101	1255										
2.																	
3.																	
4.																	
5.																	
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.												
1	.14	514	1.30	.980	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.												
2.					Specific Gravity Separator Gas _____ X X X X X X X X X												
3.					Specific Gravity Flowing Fluid _____ X X X X X												
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.												
5.					Critical Temperature _____ R _____ R												
F _c 2117 P _c ² 4481689					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0322$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0241$												
NO.	P _f	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1285$												
1		374	139876	4341813													
2																	
3																	
4																	
Absolute Open Flow 1285					Mcf @ 15.025					Angle of Slope @					Slope, n .75		
Remarks:																	
Approved By Division				Conducted By:				Calculated By:				Checked By:					