

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
Firm Copy
Revised 9-1-65

JUL 31 1969

**OIL CON. COM.
DIST. 3**

Type Test:		☒ Initial		☐ Annual		☐ Special		Test Date		7-23-69				
Company				Connection										
Aztec Oil & Gas Company				Southern Union Gas										
Pool				Formation				Unit						
				Pictured Cliffs										
Completion Date			Total Depth			Plug Back TD			Elevation			Form or Lease Name		
7-16-69			2162			2152			5868 GR			Cain		
Casing Size		Wt.		d		Set At		Perforations:				Well No.		
4-1/2"		9.5		4.090		2152		From 2011 To 2035				9		
Tubing Size		Wt.		d		Set At		Perforations:				Unit Sec. Twp. Rge.		
1.315		1.7		1.049		2017		From opened To				16 28N 10W		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple								Packer Set At		County				
Single										San Juan				
Producing Data				Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State				
										New Mexico				
L		H		Gg		% CO ₂		% N ₂		% H ₂ S		Prover		
												Water Run Taps		

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	2	X	3/4				508		512		
2.							201		188		
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Comp. Factor Fpv	Rate of Flow Q, Mscf
1.	12.365		200	1.000	.9258	1.032	2359
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	
					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
1.					Specific Gravity Separator Gas _____ X X X X X X X X	
2.					Specific Gravity Flowing Fluid _____ X X X X X	
3.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.	
4.					Critical Temperature _____ R _____ R	
5.						

P _c 524	P _c ² 274576	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1818$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1525$
NO.	P _r ²	P _w	P _r ² - P _w ²
1.	40000	206	42244
2.			
3.			
4.			
5.			

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2719$$

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Absolute Open Flow	2719	Mscf @ 15.025	Angle of Slope θ	Slope, n
Remarks:				
Approved By Commission:	Conducted By:	Calculated By:	Checked By:	