NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 8-13-77	
Company: Getty Oil Company			Connection: Not Connected		
Pool: Aztec			Formation: Pictured Cliffs		Unit
Completion Date: 8-8-77	Total Depth: 1966		Plug Back TD: 1926	Elevation: 5693	Farm or Lease Name: Mexico Federal "B"
Csg. Size: 5.500 / Wt.: 14.0 / d: 5.012 / Set At: 1961			Perforations: From 1861 To 1897		Well No.: 1 A
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 1837			Perforations: From Open To Ended		Unit: M / Sec.: 9 / Twp.: 28N / Rge.: 10W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Gas ;Gas Multiple			Packer Set At: 1837		County: San Jaun
Producing Thru: Tubing	Reservoir Temp. °F: @	Mean Annual Temp. °F	Baro. Press. – P_a		State: New Mexico
L: 1825 / H: 1825 / Gg: .645	% CO_2	% N_2	% H_2S	Prover: 2.000	Meter Run / Taps

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI							258				168 Hr.
1.	2.000	x	.750				27	60			1 Hr.
2.	2.000	X	,750				25	60			1 Hr.
3.	2.000	x	.750				25	60			1 Hr.
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		39	1.000	1.241	1.007	536
2.	11.00		37	1.000	1.241	1.007	508
3.	11.00		37	1.000	1.241	1.007	508
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 270 P_c^2 72900

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1				
2				
3	1369	57	3249	69651
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0466$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0394$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 528$

Absolute Open Flow 528 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .85

SEP 1977 OIL CON. COM. DIST. 3

Remarks: _____

Approved By Commission: _____ Conducted By: Paul D Berhost Calculated By: Paul D Berhost Checked By: _____