STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 3/22/83	
Company: Union Texas Petroleum Corp.	Connection: Southern Union Gathering Company			
Pool: Basin	Formation: Dakota		Unit	
Completion Date: 2/12/83	Total Depth: 6580	Plug Back TD: 6482	Elevation: 5799	Farm or Lease Name: Congress Lachman
Csg. Size: 9.625 / 7.000 — Wt.: 36.00 / 23.00 — d: 8.921 / 6.366 — Set At: 5348 / 5124-6580		Perforations: From 6294 To 6403		Well No.: 4-E
Tbg. Size: 2.375 — Wt.: 4.70 — d: 1.995 — Set At: 6348		Perforations: Open-Ended From To		Unit: C — Sec.: 18 — Twp.: 28N — Rge.: 10W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Dual - Gas - Oil		Packer Set At: 6060		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F: e	Mean Annual Temp. °F	Baro. Press. – P_a: 12	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
6338		0.650						

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2"	3/4"				575				7 Days
1.						15	58°			3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		27	1.0019	0.9608	1.000	321
2.							
3.							
4.							
5.							

NO.	P_r	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 587 P_c^2 344,569

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1			3088	341,481
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0090$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0067$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 323$

Absolute Open Flow 323 Mcfd @ 15.025 | Angle of Slope θ _____ | Slope, n 0.75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Clifton Gates	Ken Roddy	

RECEIVED
OIL CON. DIV.
DIST. 3