

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☒ Special					Test Date 2-16-82				
Company Amoco Production Company				Connection El Paso Natural Gas Company					
Pool Basin				Formation Dakota				Unit	
Completion Date 12-16-82		Total Depth 6190		Plug Back TD 6154		Elevation 5541 GL		Farm or Lease Name Gallegos Canyon Unit	
Csg. Size 5.500	Wt. 17	d 4.892	Set At 6190	Perforations: From 5950 To 6080			Well No. 217E		
Tng. Size 2.375	Wt. 4.7	d 1.995	Set At 6093	Perforations: From open To ended			Unit Sec. Twp. Rge. D 13 28N 12W		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual (Commingled)*					Packer Set At 5900		County San Juan		
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	13 Days						817		X		
1.	2.375	.750					225		X		3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		237	1.000	.9258	1.028	2789
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 829	P _c ² 687241					
NO.	P _t	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1216$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0899$
1		273	74529	612712		
2						
3						
4						
5						

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3040$$

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.1216$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0899$$

Absolute Open Flow	3040	Mcf/d @ 15.025	Angle of Slope @	Slope, n .75
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Remarks: Sliding sleeve at 5900' (Gallup)
 *W/O commingled orders

Approved by Commission	Conducted By J. J. Barnett	Calculated By J. J. Barnett	Checked By QB
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