3-MMCC Astec 1-Mill Cutler 1-Cliver Fowler 1-L. D. Gelloway 1-Wayne Smith 1-File

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

		Fo	rmation	lies	a Verde		County	Rio Ar	ribe
nitial									
ompany PACIFIC									
nit <b>K</b> S			,						
sing <b>51"</b> W	<del></del>								
bing1-1/4" W									
s Pay: From_									
oducing Thru: te of Complet									
•			<del></del>		ED DATA	<del></del>	- <b>-</b>		
sted Through	(PHHHH)	(Choke)	(MALAL)	Elmt	in 7 day	78	Type Tan	s	
	Flow I				Tubing		Casing I	ata	
(Prover)	(Choke) (Orifice)	Press.	1	_	Press.	Temp.	Press.	Temp.	Duration of Flor
Size	Size	psig	h <sub>w</sub>	°F.	psig	o <sub>F</sub> .	psig	<sup>⊃</sup> F•	Hr.
	3/4"	415		73	1031		1103 415	73	3
Coefficient $(24-\text{Hour}) \qquad \sqrt{\text{h}_{\text{W}}}$ 12.3650		v <sup>p</sup> f	Pressure psia		Flow Temp. Factor Ft		Compress. Factor Fpv 1.040		Rate of Flow Q-MCFPD @ 15.025 psi
14,370		<b>_</b>		1241		9608			
12.3650									
			DDI	regimer o	CALCULATIO	ONS	<del></del>		
		١		cf/bbl.					rator Gas
vity of Liqui	d Hydrocar	oons		deg.		Speci P.	fic Gravi <b>1115</b>	P2 :	1243.2
vity of Liqui	d Hydrocar					Speci P <sub>c</sub>	fic Gravi	Pc	1243.2
vity of Liqui	d Hydrocar	oons(1-e <sup>-s</sup> )_		deg.	-	Speci P <sub>c</sub>	fic Gravi	P <sub>c</sub>	
P <sub>w</sub> Pt (psia)	d Hydrocar	oons		deg.	F <sub>cQ</sub> ) <sup>2</sup>	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub>	_P <sup>2</sup>	Pw Pc
Pt (psia)	d Hydrocar	oons(1-e <sup>-s</sup> )_		deg.	FcQ) <sup>2</sup>	P <sub>c</sub>	1115	_P <sup>2</sup>	ıl. P <sub>w</sub>
vity of Liqui	d Hydrocar	oons(1-e <sup>-s</sup> )_		deg.	FcQ) <sup>2</sup>	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub>	_P <sup>2</sup>	Pw Pc
Pw Pt (psia)	d Hydrocarl	cons (1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	deg.	CcQ) <sup>2</sup>	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	_P <sup>2</sup>	Pw Pc
Pw Pt (psia)  solute Potent	d Hydrocar	cons (1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	deg. (F) (I) MCFPD;	FcQ) <sup>2</sup> -e-s)	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	_P <sup>2</sup>	Pw Pc
Pw Pt (psia)  solute Potent MPANY DRESS ENT and TITLE	Pt ial: 6	oons (1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	deg.  (F) (1)  MCFPD;	F <sub>c</sub> Q) <sup>2</sup> -e <sup>-s</sup> )  n -7:	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	_P <sup>2</sup>	Pw Pc
Pw Pt (psia)  solute Potent MPANY	Pt in the state of	FcQ	(F <sub>c</sub> Q) <sup>2</sup>	deg.  (F (1)  MCFPD;	CQ) <sup>2</sup> -e-s) n •7	P <sub>c</sub>	P <sup>2</sup> -P <sup>2</sup> <sub>w</sub>	Pc	Pw Pc
Pw Pt (psia)  solute Potent MPANY PACIFIC ENT and TITLE	Pt in the state of	FcQ	(F <sub>c</sub> Q) <sup>2</sup>	deg.  (F)  (I)  MCFPD:	F <sub>c</sub> Q) <sup>2</sup> -e <sup>-s</sup> )  n -7:	P <sub>c</sub>	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Pc Ca	Pw Pc

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 600 F.
- $P_c$ = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_{t-}$  Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- $h_{\mathbf{w}}^{-}$  Differential meter pressure, inches water.
- Fg Gravity correction factor.
- $F_{t}$  Flowing temperature correction factor.
- $F_{\text{DV}}$  Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .

OIL CONSERV	ATION COMMISSION
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