

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLForm C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4-26-73	
Company Lively Exploration Co.				Connection	
Pool Boson Dakota				Formation Dakota	
Completion Date 4/15/73		Total Depth 7615		Plug Back TD 7582	
Elevation 6514.66		Farm or Lease Name Lively			
Casing Size 4 1/2"		Wt. 21.2		Set At 7614	
Perforations: From 7342 To 7582		Well No. 6			
Teg. Size 1 1/4"		Wt. 2.4		Set At 7446	
Perforations: From Open End To		Unit G-30 29H 8W			
Type Well - Single - Bracenehead - G.G. or G.O. Multiple Single Gas				Packer Set At	
Producing Thru TLG				County San Juan	
Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a	
State New Mexico					
L		H		G _g	
% CO ₂		% N ₂		% H ₂ S	
Prover		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.							2202		2247		7402
2.	3/4" Pro. CL.			122		500			1550		5442
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.							
2.	12.365		172	10078	.9601	1.012	2174
3.							
4.							
5.							

NO.	P _r	Temp. °R	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.			A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.			Specific Gravity Separator Gas _____ XXXXXXXXXX
3.			Specific Gravity Flowing Fluid _____ XXXXXX
4.			Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.			Critical Temperature _____ R _____ R

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OIL CON. COM.

DIST. 3

NO.	P _r ²	P _w ²	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1.					1.9161	1.6286
2.		1312	5,457,770	2,442,207		
3.						
4.						
5.						

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3541$

$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.9161$

$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.6286$

Absolute Open Flow	3541	Mcf @ 15.025	Angle of Slope °	Slope, n	.75
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Remarks:			
Approved By Commission:	Conducted By:	Calculated By:	Checked By: