

3 - N.M.O.C.C. (Aztec)  
1 - L. G. Truby NEW MEXICO OIL CONSERVATION COMMISSION  
1 - W. R. Johnston  
1 - Stanolind Gas (Farm.)  
1 - File

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Blanco Formation Mesaverde County Rio Arriba  
Initial XX Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 8-7-56  
Company Pacific Northwest Pipeline Corp. Lease Rosa Well No. 14-23  
Unit B Sec. 23 Twp. 31N Rge. 6W Purchaser not connected  
Casing 5" Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at 5,739 Perf. \_\_\_\_\_ To \_\_\_\_\_  
Tubing 2" Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at 5,689 Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 5,728 To 5,378 L \_\_\_\_\_ x Gest .670 -GL \_\_\_\_\_ Bar.Press. 12.0  
Producing Thru: Casing \_\_\_\_\_ Tubing XI Type Well Single  
Single-Bradenhead-G. G. or G.O. Dual  
Date of Completion: \_\_\_\_\_ Packer \_\_\_\_\_ Reservoir Temp. \_\_\_\_\_

OBSERVED DATA

Tested Through ~~00000000~~ (Choke) ~~00000000~~ Type Taps \_\_\_\_\_

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) <del>00000000</del> Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						1,115		1,115		Shut-in
1.										
2.		2 x 3/4	261		91	261	91	641		3 hr. flow
3.										
4.										
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wp}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.							
2.							
3.	12.3650		273	.9745	.9463	1.023	3,175
4.							
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ deg.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> \_\_\_\_\_ (1-e<sup>-S</sup>)  
Specific Gravity Separator Gas \_\_\_\_\_  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 1,127 P<sub>c</sub> 1270.1

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> )	P <sub>c</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> /P <sub>c</sub>
1.									
2.									
3.						426.4	843.7		1.505
4.									
5.									

Absolute Potential: 4315 MCFPD; n .75 = 1.359

COMPANY Pacific Northwest Pipeline Corp.

ADDRESS 405 1/2 West Broadway, Farmington, New Mexico

AGENT and TITLE W. B. Richardson, III; Well Test Engineer

WITNESSED \_\_\_\_\_

COMPANY \_\_\_\_\_

REMARKS \_\_\_\_\_



## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_{w-}$  Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P<sub>t</sub> = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  - Supercompressibility factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .

FEDERAL CONSERVATION COMMISSION		
AZTEC DISTRICT OFFICE		
RECEIVED		
DATE	FILE	
10/10/50	1	
FILE	1	✓