

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1965

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10/30/78			
Company AMOCO PRODUCTION COMPANY				Connection NORTHWEST PIPELINE CORPORATION					
Pool BASIN				Formation DAKOTA				Unit	
Completion Date 10/5/78		Total Depth 8118		Plug Back TD 8070		Elevation 6397		Farm or Lease Name ROSA UNIT	
Csg. Size 4.50	Wt. 11.6	d 4.00	Set At 8108	Perforations: From 7950 To 8014		Well No. 64			
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 8021	Perforations: From Open To Ended		Unit A		Sec. 29	Twp. 31
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At None		County Rio Arriba	
Producing Thru Tubing		Reservoir Temp. °F 8		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L	H	G _g .70	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	7 days						2280		2280		
1.	2.375		0.750				102	60	1360		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		114	1	.9258	1.012	1321
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 2292	P _c ² 5253264			(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.5584}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.3948}$
NO.	P _t	P _w	P _w ²	P _c ² - P _w ²	
1		1372	1882384	3370880	
2					
3					
4					
5					

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1843}$

Absolute Open Flow 1843	Mcf @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks: _____

Approved by Commission	Conducted By: RAC	Calculated By: R. A. Conner	Checked By: J. L. Krupka
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