

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☒ Special				Test Date 10/3/84		OCT 19 1984	
Company Amoco Production Company				Connection Northwest Pipeline Corporation			
Pool Undesignated				Formation Gallup		Unit DIST. 3	
Completion Date 8/28/84		Total Depth 8127		Plug Back TD 8070		Elevation 6387GL	
Form or Lease Name Rosa Unit		Well No. 100		Unit N		Sec. Twp. Rge. 21 31 6	
Crg. Size 4.500		Wt. 11.6		Set At 8127		Perforations: From 7092 To 7300	
Tbg. Size 2.375		Wt. 4.7		Set At 7313		Perforations: From sliding To sleeve	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single-Commingle				Packer Set At 7348		County Rio Arriba	
Producing Thru tubing		Reservoir Temp. °F 8		Mean Annual Temp. °F		Baro. Press. - P _a New Mexico	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	15 days						2840		2840	
1.	2.375		.500				410		995	38 hrs.
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	5.4315		422	1.000	.9258	1.052	2232
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 2852	P _c ² 8133904	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1424$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1050$
NO.	P _r ²	P _w ²	P _w ² - P _r ²
1		1007	1014049
2			
3			
4			
5			

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2466$

$AOF = Q = 2466$

Absolute Open Flow	2466	Mcfd @ 15.025	Angle of Slope θ	Slope, n = .75
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Remarks: Not flared, heavy spray H₂O

Approved By Consultant	Conducted By J. Barnett	Calculated By J. Barnett	Checked By
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