

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☒ Special				Test Date 12/11/84		JAN 28 1985	
Company Amoco Production Company				Connection Northwest Pipeline Corp.			
Pool Basin				Formation Dakota		Unit Dist. 7	
Completion Date 10/26/84		Total Depth 8109		Plug Back TD 8060		Elevation 6253 GR	
Csg. Size 4.500		Wt. 11.6		Set At 4.000		Perforations: From 7810 To 7907	
Tbg. Size 2.375		Wt. 4.7		Set At 1.995		Perforations: From open To ended	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Commingle				Packer Set At 7240		County Rio Arriba	
Producing Thru tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a	
L		H		G _g		% CO ₂	
						% N ₂	
						% H ₂ S	
						Prover	
						Meter Run	
						Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	38 days						2835		X		
1.	2.375		.750				140		X		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		152	1.000	.9258	1.017	1770
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P_c 2847					P_c^2 8105409	$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.0035}{}$	$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.0027}{}$
NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$			
1		169	28561	8076848			
2							
3							
4							
5							
AOF = Q						$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1775}{}$	

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1775$$

Absolute Open Flow 1775 Mcfd @ 15.025		Angle of Slope @ _____		Slope, n .75	
Remarks: flared, heavy H ₂ O sliding sleeve set @ 7234					
Approved By Commission:		Conducted By: J.J. Barnett		Calculated By: J.J. Barnett	
				Checked By:	