STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

RECEIVED
MAR 14 1985
OIL CON. DIV.
DIST. 3

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Type Test: [x] Initial [ ] Annual [ ] Special			Test Date: 2-8-85	
Company: Amoco Production Co.	Connection: Northwest Pipeline			Unit
Pool: undes.	Formation: Gallup			
Completion Date: 1-2-85	Total Depth: 3488	Plug Back TD: 8430	Elevation: 6620 GR	Farm or Lease Name: Rosa Unit
Csg. Size: 4.500 / Wt.: 11.6 / d: 4.000 / Set At: 8488		Perforations: From 7216 To 7620		Well No.: 109
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 7775		Perforations: From sliding To sleeve		Unit: M / Sec.: 9 / Twp.: 31 / Rge.: 5
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: commingle		Packer Set At: 7768		County: Rio Arriba
Producing Thru: tubing	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI	9 days						2511		2560		
1.	2.375		.750				143		1286		3hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12,365		155	1.000	.9258	1.017	1805
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 2572 P_c^2 6615184

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		1298	1688(4	4930380
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3417$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.2467$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2250$

Absolute Open Flow 2250 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .75

Remarks: dry gas thur test

Approved By Division	Conducted By:	Calculated By:	Checked By:
	B&R services	JJ Barnett	