

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool BASIN DAKOTA Formation DAKOTA County SAN JUAN

Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 1-10-63

Company TENNECO OIL COMPANY Lease BASSETT GAS UNIT Well No. 1

Unit \_\_\_\_\_ Sec. 33 Twp. 30 Rge. 10 Purchaser \_\_\_\_\_

Casing 5.5 Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at \_\_\_\_\_ Perf. 7038 To 7108

Tubing 2-3/8 Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at 7027 Perf. \_\_\_\_\_ To \_\_\_\_\_

Gas Pay: From \_\_\_\_\_ To \_\_\_\_\_ L 0.65 xG \_\_\_\_\_ -GL \_\_\_\_\_ Bar.Press. 12.0

Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Single Gas

Date of Completion: \_\_\_\_\_ Packer \_\_\_\_\_ Single-Bradenhead-G. G. 185 G.O. Dual Reservoir Temp. \_\_\_\_\_

## OBSERVED DATA

Tested Through XXXXXXX (Prover) XXXXXXX (Choke) XXXXXXX (Meter) Type Taps \_\_\_\_\_

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
1.	<u>3/4</u>					<u>1965</u> <u>227</u>	<u>78</u>	<u>1968</u> <u>760</u>		<u>3 Hours</u>
2.										
3.										
4.										
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	<u>12.3650</u>		<u>239</u>	<u>0.9531</u>	<u>0.9568</u>	<u>1.022</u>	<u>2853</u>
2.							
3.							
4.							
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.

Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.

F<sub>c</sub> \_\_\_\_\_ (1-e<sup>-s</sup>)

Specific Gravity Separator Gas \_\_\_\_\_

Specific Gravity Flowing Fluid \_\_\_\_\_

P<sub>c</sub> 1980 P<sub>c</sub> 3920/100

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub> P <sub>c</sub>
1.	<u>772</u>					<u>595984</u>	<u>3324416</u>	
2.								
3.								
4.								
5.								

Absolute Potential: 3228MCFPD; n 0.75 (1.1314)

COMPANY Tenneco Corp., acting by its managing agent, Tenneco Oil Company

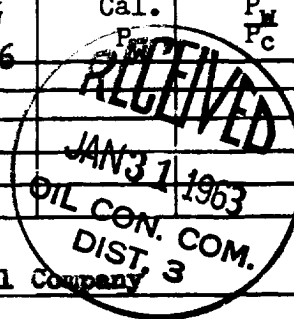
ADDRESS P. O. Box 1714, Durango, Colorado

AGENT and TITLE L. B. Plumb, District Petroleum Engineer

WITNESSED \_\_\_\_\_

COMPANY \_\_\_\_\_

REMARKS



## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .