3-000 - 1-Bill Parrish 1-Tidewater, Durango, 2-Midland 1-NW---1-Lion 1-Texas Nat'1. NEW MEXICO OIL CONSERVATION COMMISSION 1-D

2

	1-F										Form C-12	
				MULTI	-POINT E	BACK PRES	SSURE TES	T FOR GA	S WELLS		Revised 12-1-5	
Pool				F	Formation Dakota				County San Juan			
											8/29/61	
									We)			
Unit	, <u>A</u>	_Sec	22 Tw	p. 301	Rg	e12	Purc	haser	El Paso N	atural G	ias Company	
Casi	ng 4½"	Wt. 10	.50# I	.D. 4.	.040 <sub>Se</sub>	t at 64	178 Pe	rf. 63	32 <b>-5</b> 2	To 64	132-52	
Tubi	ng 11 m	_Wt2	2.70# <sub>I</sub>	.D. 1	.610 <sub>Se</sub>	t at	113 Pe	rf	فالموس والمستقدم والمستود والمستقدم والمستقدم والمستقدم والمستقدم والمستقدم والمستقدم	To64	113	
Gas	Pay: Fro	m633	2 To_	6452	L <b>6</b>	413 ,	.G67		4296.7	_Bar.Pre	ess. 12.0	
Prod	ucing Thr	ru: Ca	sing_		Tu	bing	X	Type W	ellenhead-G.	Single-G	as	
Date	of Compl	etion:_	8/12	/61	Packe	r	Sin	gle-Brad Reserv	enhead-G. oir Temp.	G. or G	.0. Dual	
							ED DATA					
Test	ed Throug	h <u>(160</u>	969CX (	Choke)	(NESSEX)				Туре Тар	os		
Flow Data							Tubing	Dat.a	Casing Data			
No.	(Prover (Line)	) (Ch			Diff.	•	Press.	Temp.	Press.	Temp.	Duration of Flow	
SI	Size	S	ize	psig	h <sub>w</sub>	°F.		°F.		°F.	Hr.	
<del>1.</del> +		<del></del>	3/4"			58	2234 210	58	2234 694	<del> </del>	7-Day 3-Hrs.	
2.				210						<b>†</b>		
3.												
<u>4.</u> 5.	<del> </del>			<b></b>					<del>}</del>	<del> </del>	· · · · · · · · · · · · · · · · · · ·	
<u> </u>				<b>!</b>			<u> </u>	L		1		
					_ 1	FLOW CAL	CULATION	5				
	Coefficient				essure		Тетр.	Gravity Compress. Rate of Flow				
No.	(2) 11-11-1		-  .			tor	Factor	Factor		Q-MCFPD		
	(24-Hour) $\sqrt{12.3650}$		√ n <sub>w</sub> i	h <sub>w</sub> p <sub>f</sub> psia		1.0019		Fg	Fpv 1.024		@ 15.025 psia	
1. 2.	12.500	<del></del>	<u> </u>		222	1.007		.9463	1.0.	24	2,665	
			<del> </del>	<del></del>							· <del></del>	
3 · 4 · 5 ·		<del> </del>	<del> </del> -									
5.												
ae I <del>-</del>	iauid Wwd	noon nho	n Datid				alcuiatio		ifia Coori	+ Como		
ravit	as Liquid Hydrocarbon Ratiocf/bbl. ravity of Liquid Hydrocarbonsdeg. c(1-e^-s)								Specific Gravity Separator Gas Specific Gravity Flowing Fluid P <sub>C</sub> 2246 P <sub>C</sub> 5044.5			
			`				•	P <sub>w</sub>	706		98.4	
No.	P <sub>w</sub>	) P.	t Fo	,Q	$(F_cQ)^2$	(F	_Q) <sup>2</sup> _e-s)	P <sub>w</sub> 2	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Ca.		
1. 2.								5044.5	4546.1		•314	
2.												
3. 4.		+							<del> </del>			
5.		<del></del>	+					· · · · · · · · · · · · · · · · · · ·	<b></b>	<del> </del>		
	14 - P	<del></del>	<del></del>	2.270			75		<u> </u>			
absol COMP <i>A</i>	Lute Poter	otial: South	West P	roducti	on Comp	MCFPD; <b>any</b>	n75			_		
ADDRE	ESS	207 F	etr. C	lub Pla	za, Far	mington,	New Mex	100	(611)	The		
AGENT	and TIT	LE	George	L. Ho	fman, J	r. Proch	iction Fo	reman	10111	/ COTY		
WITNE	ESSED								15PAP.			
COMPA	NY								SEP11	1961		
						REM	ARKS		OIL SOF	MCO L	J	
								`	OIL COM	r. 3 /	,	

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure ( $P_W$ ). MCF/da. @ 15.025 psia and 600 F.
- $P_c$ = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt\_Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- $h_{\mathbf{W}}^{-}$  Differential meter pressure, inches water.
- $F_g = Gravity$  correction factor.
- $F_t$  Flowing temperature correction factor.
- $F_{\mathrm{DV}}$  Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .

