Pool Rienco

NEW MEXICO OIL CONSERVATION COMMISSION

y		NEW	MEXIC	o oli	L CON	SERVATIO	N COMMISS	ION				V
											Form	C-122
	MU	LTI.	-POINT	BACK	C PRES	SSURE TES	ST FOR GA	S WELLS		Revis	ed 1	2-1-55
		Fo	ormati	on	Mes	. Verde		County_	Sen.	Juan		
Anı	nual				_Spec	ial		Date of	Test_	2-28-5	8	
es i	PIPE	TATE	<u> </u>	Lea	se	Blanco	31-8	We	ll No.	5-26		
7	ľwp	31.1		Rge	8w	Purc	haser	not com	betse			
	I.D.			Set a	.t_ <u>57</u>	00' 40' Pe	erf 513	101	То	56401		
											3	2
				[ubi.n	g:	X X	Type We	ell 85 enhead-G. oir Temp.	ngle	0 0 0		
<i>H</i>	3/4 (Chok	(e)		0	BSERV	ATAG GE		Туре Тај				
.QW	<u>Data</u>					Tubing	Data	Casing I	ata			$\overline{}$
ce)	Pre	ess.	Diff	T	emp.	Press.	Temp.	Press.	Temp	-]	Durat	ion

Ini	itial XX		Annu	ual		Spe	cial		Date of	Test_2	2-28-58
Con	npany Plant	C HORT	BIEST I	PIPELII	E	_Lease	Blanco	31-8	Wel	L1 No5	j -26
Uni	it <u>G</u>	_Sec. 2	<u>5</u> Tw	љ. <u>31</u> 1	R _{	ge. 8 W	Pur	chaser	not com	ected	
Cas	it G 7-5/8 " sing 5-3 "	_Wt	I	.D	Se	35 et at_ <u>57</u>	100' 140' Pe	erf. 513	0'	То	5640'
	oing 1-1/4"										
Gas	Pay: From	a 51 30'	To_	5640'	L		kG .650			Bar.Pr	ess. 12
	oducing Thru										
Dat	e of Comple	tion:_			Packe	er	Sin	ngle-Brade Reservo	enhead-G. oir Temp	G. or C	3.0. Dual
							ED DATA				
Tes	ted Through	ı LEHA	tett (3/4"T. Choke)	. C. <i>(Yeşeş)</i>	Shat	i 1 2 13 d	878	Туре Тар	·s	
			Flow Da								-
$\overline{}$	(Prover)				Diff.	Temp.		Data Temp.	Casing D		j Dumaki am
No.	(Line) Size	(Ori	fice)	psig		o _F .				Temp.	of Flow
0.7			IZE	herR	h _w	r.	psig	F.	psig	F.	Hr.
SI 1.		+		300	 	48	1077	480	110	ļ	
2.		3/4		122	 	40	122	40	1037	ļ	3 hours
<u>3.</u>		+			 		ļ	 			
4.		T		 	 	 				 	
4. 5.										 	
										·	
	Coeffic			——————————————————————————————————————		FLOW CAL					
No.	COGITIC.	lent		Pr	ressure			Gravity			Rate of Flow
1.01	(24-Ho	וור)	√ h _w p	_	psia			Factor F			Q-MCFPD
1.	-		V "WP					Fg	Fpv		@ 15.025 psia
	12.3650		 		134	1.01	.7	.9698	1.0	13	1632
2. 3. 4.			 		+						
4.											
5.											
											 -
					PRI	ESSURE CA	ALCUTATION	ONS			
as I	Liquid Hydro	oca rhor	. Ratic			cf/bbl.		Speci	eia Coordi	Comn	
	ity of Liqui					deg.			fic Gravit		rator Gas ring Fluid
				-e ^{-s})					110 Gravit	P _c 12	
								- c—		-¹ C 	
T	P _w		. T					100		 	
No.		P _t ²	Fc	Q	$(F_cQ)^2$	(F,	cQ) ² -e-s)	* P. 2	$P_c^2 - P_w^2$	Cal	1. P.
	Pt (psia)					(1:	-e-s)			P,	$\begin{array}{c c} P_{\mathbf{W}} \\ \hline P_{\mathbf{C}} \end{array}$
1. [L						1160.4	130.4		8.95

No. Pt (psia)	Pt ²	F _c Q	$(F_cQ)^2$	$(F_cQ)^2$ $(1-e^{-s})$	10kg	$P_c^2-P_w^2$	Cal.	Pw Pc
1.					1160.4	138.4		8.95
2.								
3.								
4.								
5.								
/bgolute Person		0 11-	<u></u>		/ r a -		<u></u>	

					
Absolute Potential:		MCFPD; n	.75/ 5.1745		
COMPANY PACTURE TO	WHER PIPELIEE CO	RPORATION			
ADDRESS 1181 West To	nedway. Parminete	m. New Mexico			 _
AGENT and TITLE	R. Hagner - Well	Test Ingineer			
WITNESSED_	ne B. Suith - Phi	llips Petroleum C	CHIPRITY		
COMPANY					·
		REMARKS		SOUTH.	

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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_W) . MCF/da. @ 15.025 psia and 600 F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- $h_{\mbox{\scriptsize W}}$ Differential meter pressure, inches water.
- Fg Gravity correction factor.
- F_t Flowing temperature correction factor.
- F_{pv} Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\mathbf{w}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{w}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.

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